

55 Craig St., Perth ON Site Plan Residential Development Servicing and Stormwater Management Report

Prepared For:

2B Developments

Prepared By:

Robinson Land Development

Project No. 24116 June 2025



TABLE OF CONTENTS

		TABLE OF CONTENTS	
LEGΔI	I NOTIF	ICATION	ı
1.0		DUCTION	
2.0		ING CONDITIONS	
3.0		LOPMENT PROPOSAL	
3.0 4.0			
4.0		R SERVICING	
	4.1	Design Criteria	
	4.2	Water Demands	
	4.2	Fire Protection	
5.0		ARY SERVICING	
	5.1	Design Criteria	
	5.2	Sanitary Demands	
6.0	STOR	M SERVICING	4
	6.1	Design Criteria	4
	6.2	Minor System	
	6.3	Major System	
	6.4	Quality Control	
7.0		ION AND SEDIMENT CONTROL	7
8.0		OVALS	
9.0		LUSIONS	
3.0	CONO		
LIST O	F TABL	FS	
	, .,		
Table 1		Pre-Development FlowsP	age 5
Table 2		5-Year Post-Development Discharge Rates	
Table 3		5-Year Post-Development Storage VolumesP	
Table 4		100-Year Post-Development Discharge RatesP	age 0
Table 5		100-Year Post-Development Storage Volumes P	
i abie c	,	100-1 ear Fost-Development Storage volumesF	age 0
LIST O	F APPE	ENDICES	
Append	A xib	Architectural Site Plan	
, ippoint	417(/ (Topographic Surveys	
		Craig St. Reconstruction plans	
		Orally St. Meconstruction plans	
Append	liv D	Existing Conditions and Removals Plan (DWG. 24116-R1)	
Append	ט אוג	Servicing Plan (DWG. 24116-S1)	
		o ,	
		Grading Plans (DWG. 24116-GR1)	
		Erosion and Sediment Control Plan (DWG. 24116-ESC1)	
		Notes & Details (DWG. 24116-N1)	
		Storm Drainage Area Plan (DWG.24116-STM1)	
A		Water Daniel Calculations	
Append	dix C	Water Demand Calculations	
		Fire Demand Calculations	
		Hydrant Coverage Sketch	
•	. 5		
Append	dix D	Sanitary Sewer Design Sheet	
Anna-	4iv ⊏	Dro. and Doot Davidonment Flavo	
Append	אוג ⊏	Pre- and Post-Development Flows	
		Storm Sewer Design Sheets	
		ICD Calculations	
		Storage Volume Calculations	
		Underground Storage System Cutsheet	

OGS Cutsheet



LEGAL NOTIFICATION

This report was prepared by Robinson Land Development for the account of 2B Developments.

Any use which a third party makes of this report, or any reliance on or decisions to be made based on it, are the responsibility of such third parties. **Robinson Land Development** accepts no responsibility for damages, if any, suffered by any third party as a result of decisions made or actions based on this project



1.0 INTRODUCTION

Robinson Land Development has been retained by 2B Developments to prepare a site servicing and stormwater management design for a proposed 3-storey residential apartment building located at 55 Craig St. in the Town of Perth, Ontario.

The client proposes to develop an approximately 1,700 m² GFA building consisting of studio, 1-bedroom, and 1-bedroom plus den apartments, along with the associated ground level parking, sidewalks, landscaping and stormwater management on the site. The site is bounded by Craig St. to the south, and single family residential properties to the east, north, and west. Refer to architectural site plan in **Appendix A** for reference.

This report will detail the proposed means of servicing the site with water and sanitary service and provide details on how to meet the Town of Perth stormwater management requirements.

2.0 EXISTING CONDITIONS

The 0.19 ha property is zoned residential (R3) and is currently unoccupied (previous single family home on the site has been demolished).

There is an imminent renewal project along Craig Street by the Town of Perth anticipated for construction Summer 2025. The renewal project is along Craig Street from Gore Street to Cole Road, and includes full replacement of the watermain, sanitary sewer, and storm sewer, as well as roadway, sidewalk, and replaced driveways up to property line. Based on correspondence with the Town, a new driveway and service laterals will be provided to the proposed 55 Craig St. development up to the property line. The following infrastructure will be provided adjacent to the site:

- 200 mm dia. PVC watermain along Craig St.
 - o A 50mm water service will be provided up to the property line of the site
- 300 mm dia. PVC sanitary sewer along Craig St.
 - A 150mm sanitary service will be provided up to the property line of the site
- 300 mm dia. PVC storm sewer along Craig St.
 - o A 200mm storm service will be provided up to the property line of the site
- A 6m wide driveway will be provided up to the property line of the site for the proposed development.

Refer to excerpts of the Craig St. Reconstruction plans (by Aplin Martin Consultants Inc., Issued for Construction, dated June 11, 2025) provided by the Town in **Appendix A** for more details. Note that the location of the services to 55 Craig St. in the Craig St. Reconstruction plans differ from those identified in the Site Servicing plan, the discrepancy has been identified with the Town and it is understood and expected the services will be installed at the location of the Site Servicing plan.

The existing grading at the north end of the site indicates stormwater runoff enters from properties east of the site and flows to properties west of the site, with a drop in elevation of approximately 1.5 m. This runoff into the property will be managed as part of the grading and on-site stormwater system Refer to the topographic surveys provided by the Owner in **Appendix A** for more details.

We noted that there was a discrepancy between locations of existing driveways of adjacent properties between the owner-provided topographic survey and the base plan of the Craig St. Reconstruction plans which was showed an overlap between the existing driveway of #59 Craig Street and the property line of #55 Craig Street. It is understood that the driveway replacements as part of the Craig St. Reconstruction project will be done at their actual



locations on site and terminate at the property line. The location of the proposed driveway and service laterals to the site shall be validated by as-built information and as part of the proposed site development to ensure integration of the proposed civil design.

3.0 DEVELOPMENT PROPOSAL

The Owner is proposing to develop the subject site into an approximately 1,700 m² GFA, 3-storey residential apartment building, consisting of studio, 1-bedroom, and 1-bedroom plus den apartments. The site will be complete with a driveway to Craig St. (tying into the driveway constructed as part of the Craig St. Reconstruction project) and site parking, including parking beneath the overhanging building. Concrete sidewalks will provide access to front and rear building entrance and to first floor apartment terraces. The building mechanical room will be provided within a basement level at the front of the building. Refer to the architectural site plan in **Appendix A** for more details.

The proposed development will be provided with water and sanitary service extensions to the building, and storm infrastructure per Town requirements. The proposed civil design drawings are provided in **Appendix B** including:

- Existing Conditions & Removals Plan
- Servicing Plan
- Grading Plan
- Notes & Details Plan
- Erosion & Sediment Control Plan
- Storm Drainage Area Plan

4.0 WATER SERVICING

4.1 Design Criteria

The subject site will receive water supply from the 200 mm watermain via the 50 mm service installed as part of the Craig St. Reconstruction project, complete with a curb stop valve at the property line. The building will not be sprinklered and therefore the service only needs to supply domestic demand.

The on-site water service has been designed according to the following standards and guidelines:

- Corporation of the Town of Perth Engineering Design Guidelines and Supplemental Specifications
- Fire Underwriters Survey (FUS) Water Supply for Public Fire Protection (2020)
- MOECC Design Guidelines for Drinking-Water Systems (2008)

Accordingly, the following watermain design criteria have been utilized for the subject site:

•	Average Daily Demand (Residential)	450 L/cap/d
•	Residential Density (1-Bedroom Apt.)	2.0 cap/unit
•	Peaking Factor (Max Day)	2.0 x Avg Day
•	Peaking Factor (Peak Hour)	2.2 x Max Day
•	Minimum Pressure During Peak Hour	275 kPa (40 psi)
•	Maximum Pressure	550 kPa (80 psi)
•	Minimum Pressure During Fire Demand	140 kPa (20 psi)



4.2 Water Demands

The domestic demands were calculated based on the above criteria and summarized below. For the purposes of demand calculations all apartment units are treated as 1-bedroom apartments. Refer to **Appendix C** for proposed domestic demand calculations.

Average Day Demand: 0.31 L/sPeak Hour Demand: 1.38 L/s

Boundary conditions were for the new watermain on Craig St. were unavailable from the Town, so head loss was calculated along the service lateral during peak hour demand scenarios using the Hazen-Williams equation.

```
\begin{array}{c} h_f = 10.67 \ ^*L \ ^*Q^{1.85} \ / \ (C^{1.85} \ ^*d^{4.87}) \\ Where \ L = 14 \ m \\ Q = 1.38 \ L/s \ (Peak \ Hour) \\ C = 100 \\ d = 50 \ mm \ (nominal) \end{array}
```

The resultant head loss along the service lateral during peak hour demand is only 0.33 m (3 kPa; 0.5 psi); therefore, provided the new watermain on Craig St. can support the minimum 275 kPa (40 psi) pressure during peak hour demands there are no concerns of the system supporting the proposed development. The system pressures on the new 200 mm watermain on Craig St. should be validated by the Town.

4.2 Fire Protection

The required fire flow for the subject site was calculated using the Fire Underwriter's Survey (FUS) long form (refer to **Appendix C**). Based on the building construction, occupancy and ground floor area, the maximum required fire flow is 15,000 L/min (250 L/s). The proposed building will not be sprinkled and fire demand will be covered by local hydrants. The nearest hydrants to the site are located at the southeast corner of Craig St. and Gore St. East and at the southwest corner of Craig St. and Drummond St. East (both within 90 m of the proposed building), which are being replaced as part of the Craig St. Reconstruction project. Refer to the hydrant coverage sketch in **Appendix C**.

Fire flow capacities for the new watermain on Craig St. were unavailable from the Town, but should be validated by the Town to confirm sufficient capacity for the proposed development.

5.0 SANITARY SERVICING

5.1 Design Criteria

Sanitary flows from the site will discharge to the 300 mm sanitary sewer on Craig St. via the 150 mm service installed as part of the Craig St. Reconstruction project.

The on-site sanitary service has been designed according to the following standards and quidelines:

- Corporation of the Town of Perth Engineering Design Guidelines and Supplemental Specifications
- MOECC Design Guidelines for Sewage Works (2008)



Accordingly, the following design parameters have been implemented for the subject site:

Average Daily Demand (Residential)
 Peaking Factor
 Infiltration Allowance
 Velocity:
 350 L/cap/d
 Harmon Equation
 0.28 L/s/ha
 0.60-3.0 m/s

5.2 Sanitary Demands

The sanitary demands were calculated based on the above criteria. For the purposes of demand calculations all apartment units are treated as 1-bedroom apartments. The peak sanitary demand was estimated to be 1.02 L/s. The sanitary service lateral has been confirmed to have capacity to convey the peak design flows and meet minimum full flow velocities. Refer to the sanitary sewer design sheet in **Appendix D** for calculation details.

Since the sanitary service provided will be entering the site above the basement elevation, a sanitary sump pump will be required within the basement mechanical room. The sanitary sump pump will be designed by the Building Mechanical Engineer during detailed design.

6.0 STORM SERVICING

6.1 Design Criteria

Stormwater runoff collected on the subject site will discharge to the 300 mm storm sewer on Craig St. via the 200 mm service installed as part of the Craig St. Reconstruction project. Stormwater runoff from properties east of the site that currently flow into the site will also be managed to not cause off-site ponding.

The storm sewer system has been designed according to the following standards and quidelines:

- Corporation of the Town of Perth Engineering Design Guidelines and Supplemental Specifications
- MOECC Stormwater Management Planning and Design Manual (2003)

Accordingly, the following design parameters have been implemented for the subject site:

Quantity Control post- to pre-development (up to 100-yr)
 Quality Control Enhanced (80% TSS reduction)

Ponding
 No ponding during 5-yr, max. 300 mm ponding

Velocity 0.80-6.0 m/s

The post-development stormwater generated by the site must be controlled to the equivalent pre-development discharge rate up to the 100-yr storm. The off-site flows entering and captured by the site are unchanged and will therefore be considered through-flows. The extents of the off-site flows that enter the site have been assumed based on the grading of Craig St., which peaks just west of Drummond St. East. Uncontrolled flows from the site that continue to drain to the property limits (the west and north perimeter of the site, and the southeast corner of the site) will be accommodated by over-control of the controlled areas. Refer to **Appendix E** for details of the calculations. The summary of the calculations are as follows:

Table 1 - Pre-Development Flows

Design Storm	Pre-Development Site Flows (L/s)	Off-Site Flows (L/s)	Total Pre- Development Flow (L/s)
5-yr	8.9	29.3	38.2
100-yr	19.1	62.6	81.7

6.2 Minor System

Stormwater runoff will be captured on site and connect to the 200 mm storm service at the property line in the centre of the proposed driveway. An oil-grit separator will be installed immediately before discharge to the storm service to provide quality control. Upstream of the oil-grit separator, an inlet control device will be installed within a maintenance hole to control the upstream runoff below maximum allowable. Upstream of the inlet control device, an underground storage system will be installed to provide quantity control up to the 100-yr storm and ensure no ponding during the 5-yr storm. The inlet control device has been sized to ensure the discharge rate is below the allowable pre-development rate, as well as capacity of the 200 mm storm service.

A 250 mm trenched storm sewer system will be installed along the east edge of the site to capture runoff from the apartment terraces and off-site runoff, connecting to a site catch basin which will capture the remainder of the off-site runoff.

The peaked-roof building will be outfitted with downspouts between the apartment units. The downspouts will be connected underground to the storm system directly to minimize runoff on hard surfaces (that create slipping hazards during shoulder seasons with intermittent freezing), along with overflows at the surface in case of backup or blockage.

Since the storm service provided will be entering the site above the basement elevation, a storm sump pump will be required within the basement mechanical room for the foundation drainage. The storm sump pump will be designed by the Building Mechanical Engineer during detailed design.

Refer to the storm sewer design sheets, ICD sizing, storage calculations, and underground storage system cutsheet in **Appendix E** for details and the Storm Drainage Area Plans in **Appendix B** for reference.

A summary of the calculations is presented in the tables below:

Table 2 – 5-Year Post-Development Discharge Rates

Area	Max Discharge Rate (L/s)
Uncontrolled	2.4
Controlled (incl. captured off-site)*	32.3
Total	34.7
5-yr Pre-Development Flow	38.2



Table 3 – 5-Year Post-Development Storage Volumes

Area	Required Storage (m³)	Available Storage (m³)
Underground Storage System	28.3	120.1

^{*}Note: Though the 5-yr controlled flow rate is noted as 32.3 L/s, this is based on the ICD flow rate when the underground storage is full. The actual flow rate during the 5-yr storm will be even less as only ~25% of the underground storage will be utilized (therefore lesser hydraulic head on the ICD)

6.3 Major System

During major storms, the storm system will still capture the storm runoff and direct it towards the underground storage system. Where pipes have insufficient capacity, spillover is expected within the site (CB1 to STMMH204), or backfeeding into the underground storage system (at STMMH203). The underground storage system has been sized to provide storage up to the 100-yr design storm, including at-grade ponding above the underground storage system. All local spillover elevations within the site are below the maximum 300 mm depth and area a minimum of 300 mm below the nearest building doorway. The ultimate site overflow route is directed to Craig St. via the site driveway.

Refer to the storm sewer design sheets, ICD sizing, and storage calculations in **Appendix E** for details and the Storm Drainage Area Plans in **Appendix B** for reference.

A summary of the calculations is presented in the tables below:

Table 3 – 100-Year Post-Development Discharge Rates

Area	Max Discharge Rate (L/s)
Uncontrolled	5.2
Controlled (incl. captured off-site)	32.3
Total	37.5
100-yr Pre- Development Flow	81.7

Table 5 – 100-Year Post-Development Storage Volumes

Area	Required Storage (m³)	Available Storage (m³)
Surface Ponding	-	12.2
Underground Storage System	-	120.1
Total	126.8	132.3



6.4 Quality Control

Quality control will be provided by an oil-grit separator downstream of the flow-controlled maintenance hole to provide quality control of the storm runoff. The oil-grit separator is sized for 80% TSS reduction based on the controlled flow rates. Refer to OGS sizing cutsheet in **Appendix E** for more details. The underground storage system design includes an "isolator row" as standard design which will also provide additional quality control, though it was not counted in the sizing of the OGS to be conservative.

7.0 EROSION AND SEDIMENT CONTROL

Prior to construction and until vegetation has been re-established in disturbed areas, erosion and sediment control measures must be implemented to mitigate the impact on receiving watercourses and existing infrastructure. Refer to the Erosion and Sediment Control Plan provided in **Appendix B** for details.

8.0 APPROVALS

The proposed development is subject to the Town of Perth Site Plan Approval and Zoning By-Law Amendment process. Further, the stormwater management system may be subject to an Environmental Compliance Approval from the Ontario Ministry of Environment, Conservation and Parks.

9.0 CONCLUSIONS

This servicing and stormwater management report has been prepared to support the Site Plan Approval and Zoning By-Law Amendment application for the development of the property located at 55 Craig Street. The report has detailed the proposed means of servicing the site for potable water and sanitary sewer and provided details on how to meet the stormwater management requirements in accordance with Town of Perth requirements. The proposed servicing and stormwater management designs will be achieved by implementing the following key features:

- Domestic water supply will be provided via the 50 mm diameter service connected to the 200 mm diameter watermain on Craig St., to be constructed as part of the Craig St. Reconstruction project.
- Fire protection will be provided by hydrants at Craig St./Gore St. E and Craig St./Drummond St. E, which are being replaced as part of Craig St. Reconstruction project.
- Sanitary flows will be conveyed to the 150 mm diameter service connected to the 300 mm diameter sanitary sewer on Craig St., to be constructed as part of the Craig St. Reconstruction project.
- Stormwater runoff (minor system) will be conveyed to the 200 mm diameter service connected to the 300 mm diameter storm sewer on Craig St., to be constructed as part of the Craig St. Reconstruction project.
- Stormwater runoff for the post-development 5-yr design storm will be controlled to the pre-development 5-yr design storm with no ponding occurring on site with on site inlet control device and underground storage system.
- Stormwater runoff for the post-development 100-yr design storm will be controlled to the pre-development 100-yr design storm. The underground storage system, as well at-grade ponding, has been designed to provide storage up to the 100-yr design storm.
- Emergency overland flows will be conveyed to Craig St. via the site driveway.
- Quality control will be provided by an oil-grit separator.



• Erosion and sediment control measures will be implemented prior to construction and maintained until vegetation has been re-established in disturbed areas.

Report Prepared By:



Stephen McCaughey, P.Eng. Project Engineer

Appendix A

Architectural Site Plan

Topographic Surveys

Craig St. Reconstruction plans (by Aplin Martin Consultants, Issued For Construction dated June 11, 2025)

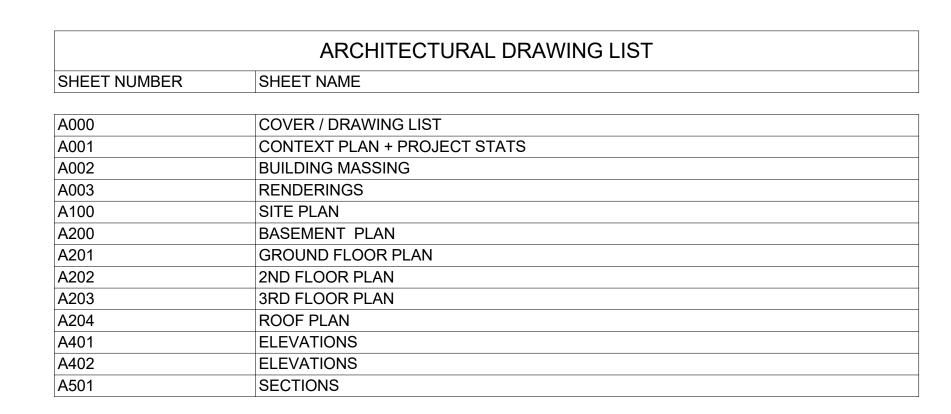
PROPOSED RESIDENTIAL DEVELOPMENT

55 CRAIG ST. PERTH, ON

2B DEVELOPMENTS

Project: 24058

Date: JUNE 2, 2025 Issued for: SPA (DRAFT)





PROJECT CONSULTANTS

ARCHITECT

RAW DESIGN INC. 22 GEARY AVE TORONTO, ON. M6H 2B4 T: 416-599-9729 F: 416-599-7729

STRUCTURAL ENGINEER

TBD

MECHANICAL & ELECTRICAL ENGINEER

TBD

CIVIL ENGINEER

ROBINSON CONSULTANS 350 PALLADIUM DRIVE, SUITE 210 OTTAWA, ON. K2V 1A8 T: 613-592-6060

TRANSPORTATION

TBD

NOISE AND VIBRATION

TBD

LANDSCAPE ARCHITECT

TB

PLANNING

WSP CANADA INC. 2611 QUEENSVIEW DRIVE, SUITE 300 OTTAWA, ON. K2B 8K2 T: 613 829-2800

ENERGY MODEL

TBD

SURVEY & TOPOGRAPHIC

CALLON DIETZ INC. 19 ROE ST, CARLETON PLACE, ON. K7C 0N3

ENVIRONMENTAL

TBD

GEOTECH / HYDRO G

TBD

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24058

55 CRAIG ST. PERTH,

PROPOSED
RESIDENTIAL
DEVELOPMENT:NTS

COVER / DRAWING LIST

SCALE:



55 CRAIG ST, PERTH PRELIMINARY SITE STATISTICS 29 May 2025

Official Plan	SITE AREA NET AREA BUILDING COVERAGE BUILDING HEIGHT	1866.0 sq.m. 1866.0 sq.m. 36% 11.5m	20,085 20,085	sq.ft. sq.ft.
Current Zoning				

AREA CALCULATIONS

	L	JNITS							GROSS F	LOOR AREA	· ·		<u></u>		OUT. AMENI	TY	GCA (INCL BAL	.C)
FLOOR		STUDIO	18	18+D	2B	3B	48	TOTAL	s COMMERCIAL	sq.ft.	s B RESIDENTIAL	sq.ft.	g ja total	sq.ft.	sq.m.	sq.ft.	sq.m.	sq.ft.
Basement									-	-	-	-		0	X#:	+	137	1,475
1		0	2	0	4	0		6	-	(*)	385	4,144	385	4,144	69	738	454	4,882
2	- 1	0	8	4	0	0		12	-	-	665	7,158	665	7,158	29	310	694	7,468
3		0	8	4	0	0		12		-	665	7,158	665	7,158	29	310	694	7,468
TOTAL Mix		O 0%	18 60%	8 27%	4 13%	O 0%	O 0%	30	0	(-	1,715	18,460	1,715	18,460	126	1,357	1,841	19,818

0.92

Outdoor Amenity			
Required (9m2/UNIT)	270	sq.m.	2,906 sq.ft.
Provided (patios+balcs+terraces)	126	sq.m.	1,357 sq.ft.
Provided (site landscaping)	324	sq.m.	3,490 sq.ft.
TOTAL PROVIDED	450	sa.m.	4,847 sq.ft.

REQUIRED		00
RESIDENT (1/UNIT??)		30.0
VISITOR (N/A)		
ACCESSIBLE (4%)		2
TOTAL	1500 NO. 100 NA. 100 N	30

20	~	E 20	
BICYCLE PARKING			
	(2005) 10 10 10 10 10 10 10 10 10 10 10 10 10	REQUIRED	PROVIDED
LONG-TERM (RESIDENTIAL)	5% required vehicular parking, minimum of 2 spaces	2.0	4.0
SHORT-TERM (RESIDENTIAL)	0	0	0.0
COMMERCIAL	0	0	0.0
TOTAL		2.2	1.0

Required Landscaped Open Space				
	Percent	sq.m.	sq.ft.	
Required	35%	653	7,030	
Provided	23%	434	4,672	

1 SITE STATISTICS A001 1:1



	UNI	T MATRIX	
Number	Name	Area	Area SF
1ST FLOOR			
101	1 BED	48 m²	513 ft²
102	2 BED (BF)	62 m²	669 ft ²
103	2 BED	62 m²	669 ft ²
104	2 BED	62 m²	669 ft ²
105	2 BED	62 m²	669 ft ²
106	1 BED	48 m²	514 ft ²
2ND FLOOR	'		
201	1 BED	45 m²	485 ft ²
202	1 BED+D	58 m²	620 ft ²
203	1 BED+D	58 m²	620 ft ²
204	1 BED+D	58 m²	620 ft ²
205	1 BED+D	58 m²	620 ft ²
206	1 BED	45 m²	485 ft ²
207	1 BED	43 m²	466 ft ²
208	1 BED	43 m²	458 ft ²
209	1 BED	43 m²	458 ft ²
210	1 BED (BF)	43 m²	458 ft ²
211	1 BED (BF)	43 m²	458 ft ²
212	1 BED	38 m²	407 ft ²
3RD FLOOR	-	1	,
301	1 BED	45 m²	485 ft ²
302	1 BED+D	58 m²	620 ft ²
303	1 BED+D	58 m²	620 ft ²
304	1 BED+D	58 m²	620 ft ²
305	1 BED+D	58 m²	620 ft ²
306	1 BED	45 m²	485 ft ²
307	1 BED	43 m²	466 ft ²
308	1 BED	43 m²	458 ft ²
309	1 BED	43 m²	458 ft ²
310	1 BED (BF)	43 m²	458 ft²

43 m²

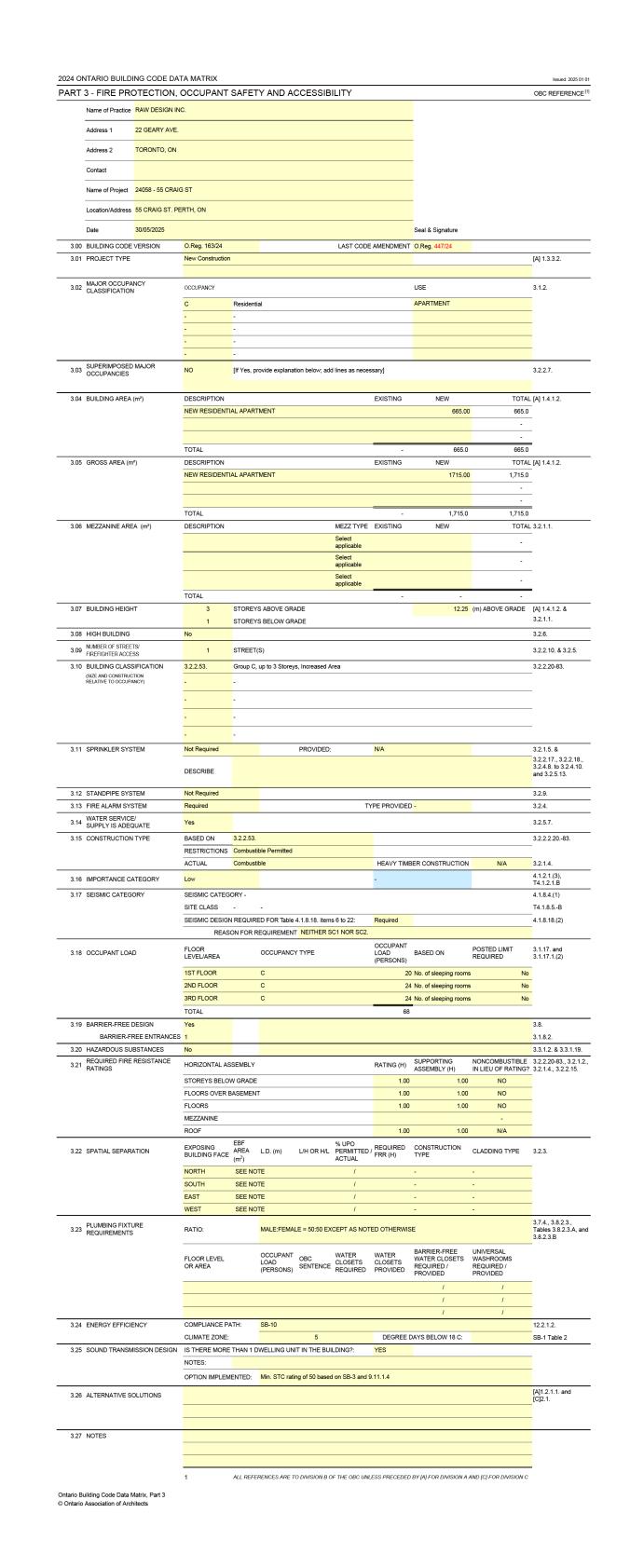
38 m²

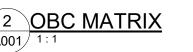
458 ft²

407 ft²

1 BED (BF)

1 BED





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-55 CRAIG ST. PERTH,

ON
PROPOSED

RESIDENTIAL DEVELOPMENT:NTS

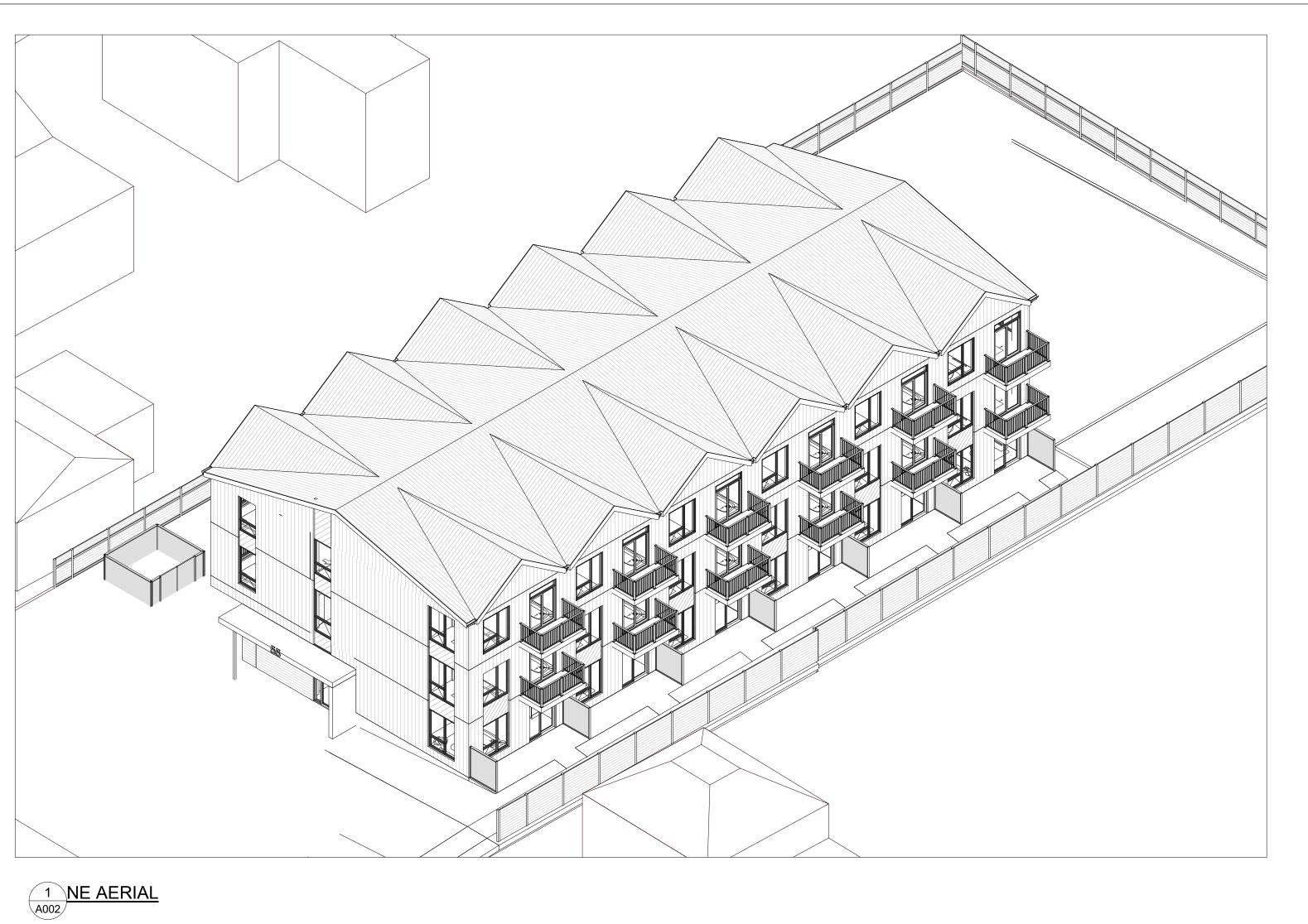
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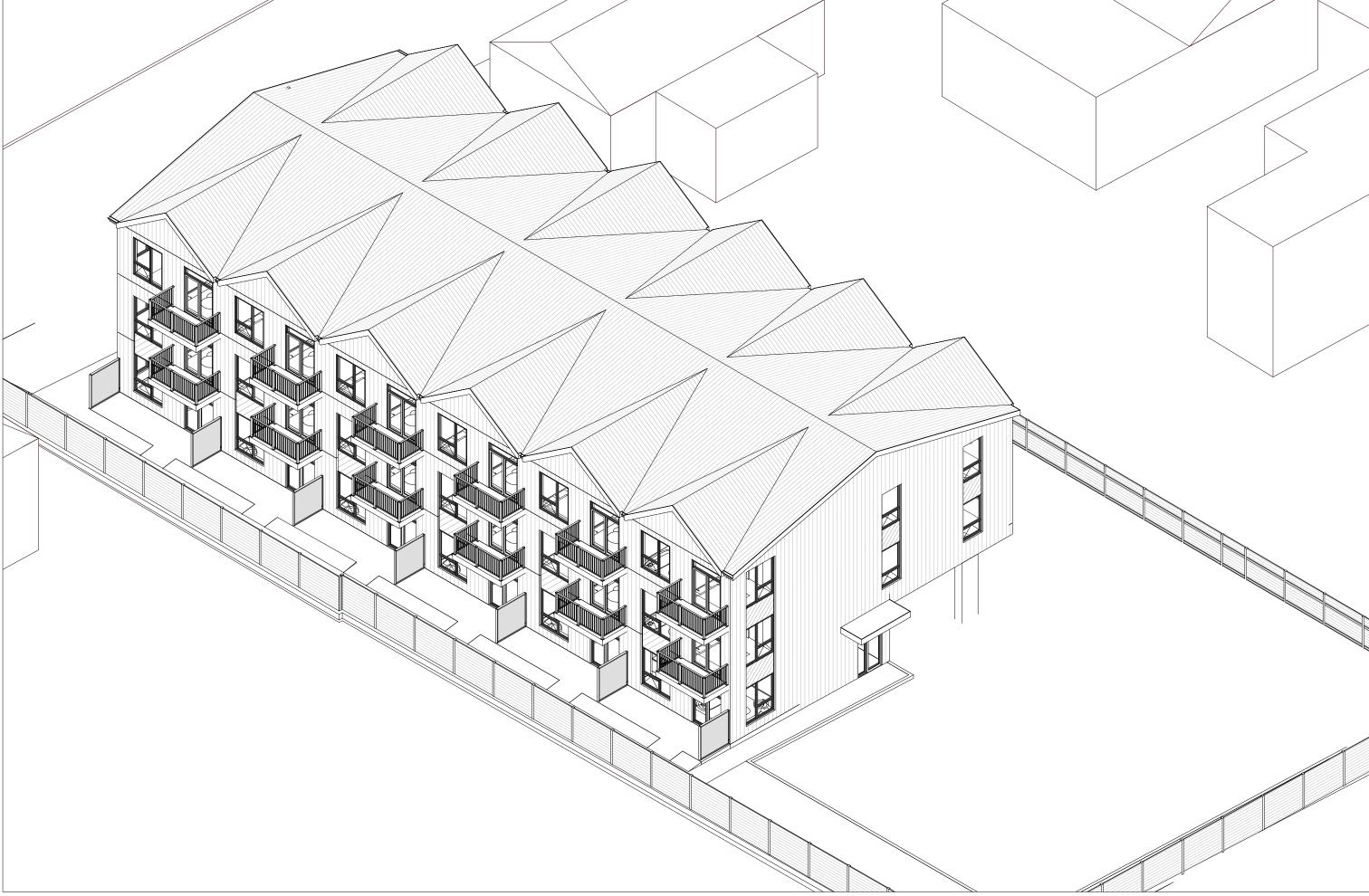
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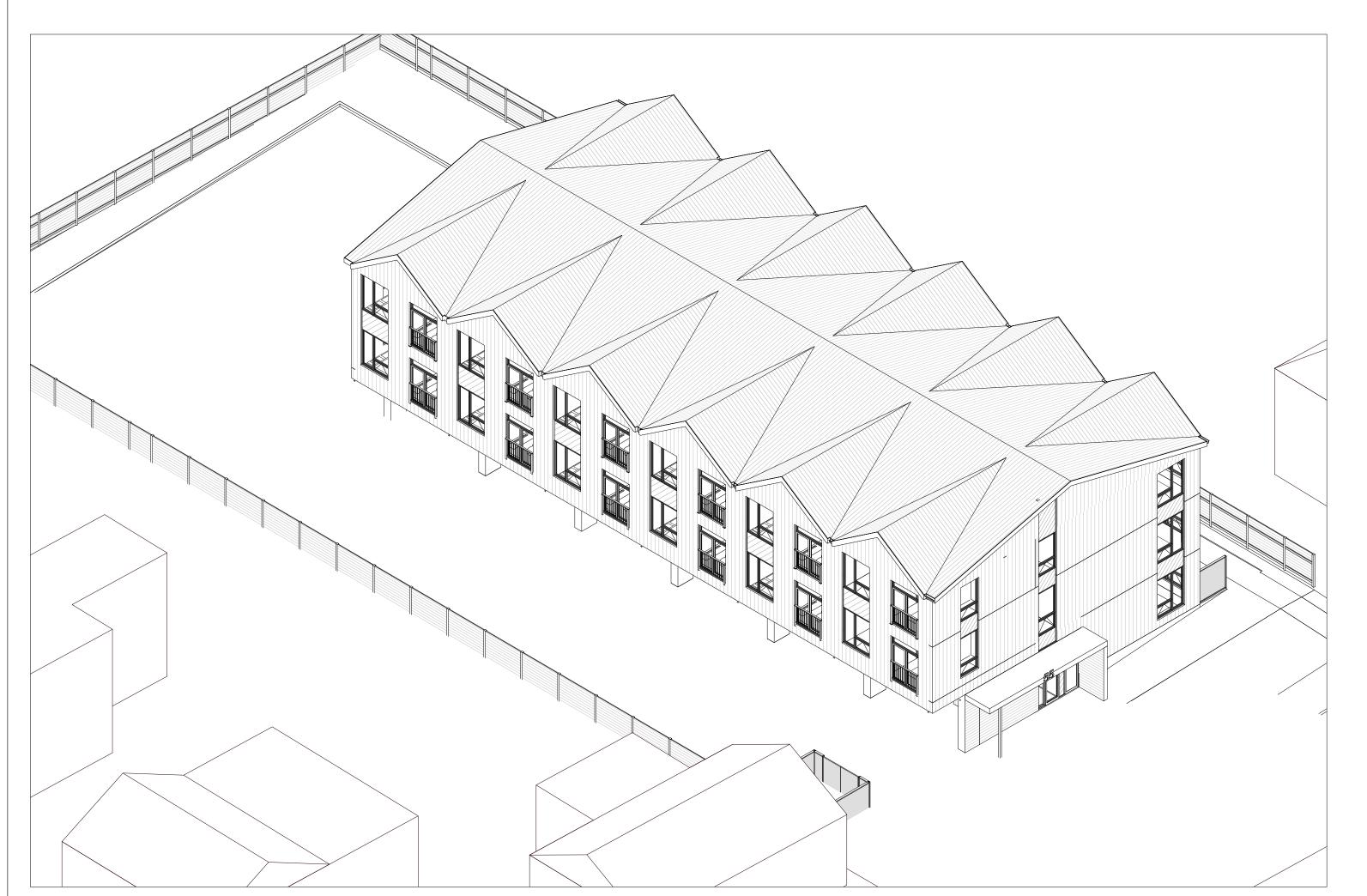
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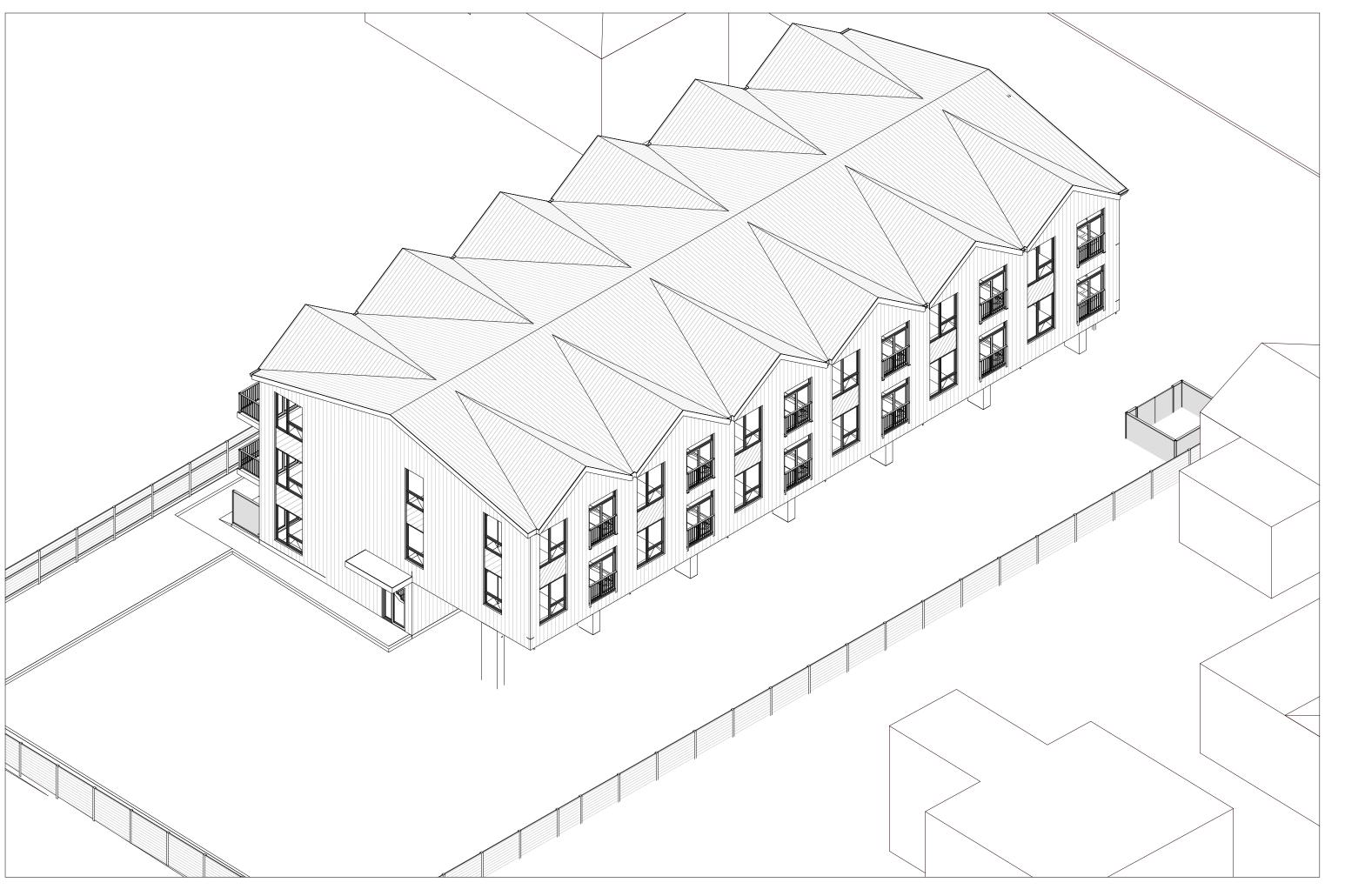
ISSUE RECORD

2025-06-02 Issued for SPA

NW AERIAL A002

4 SW AERIAL





405-317 ADELAIDE STREET WEST TORONTO CANADA M5V 1P9 +1 416 599 9729 WWW.RAWDESIGN.CA

- 24058

55 CRAIG ST. PERTH, ON

PROPOSED
RESIDENTIAL
DEVELOPMENT:NTS

– BUILDING MASSING

SCALE:

A002

3 SE AERIAL





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NO. DATE DESCRIPTION









405-317 ADELAIDE STREET WEST TORONTO CANADA M5V 1P9 +1 416 599 9729 WWW.RAWDESIGN.CA

24058

55 CRAIG ST. PERTH, ON

PROPOSED RESIDENTIAL DEVELOPMENT:NTS

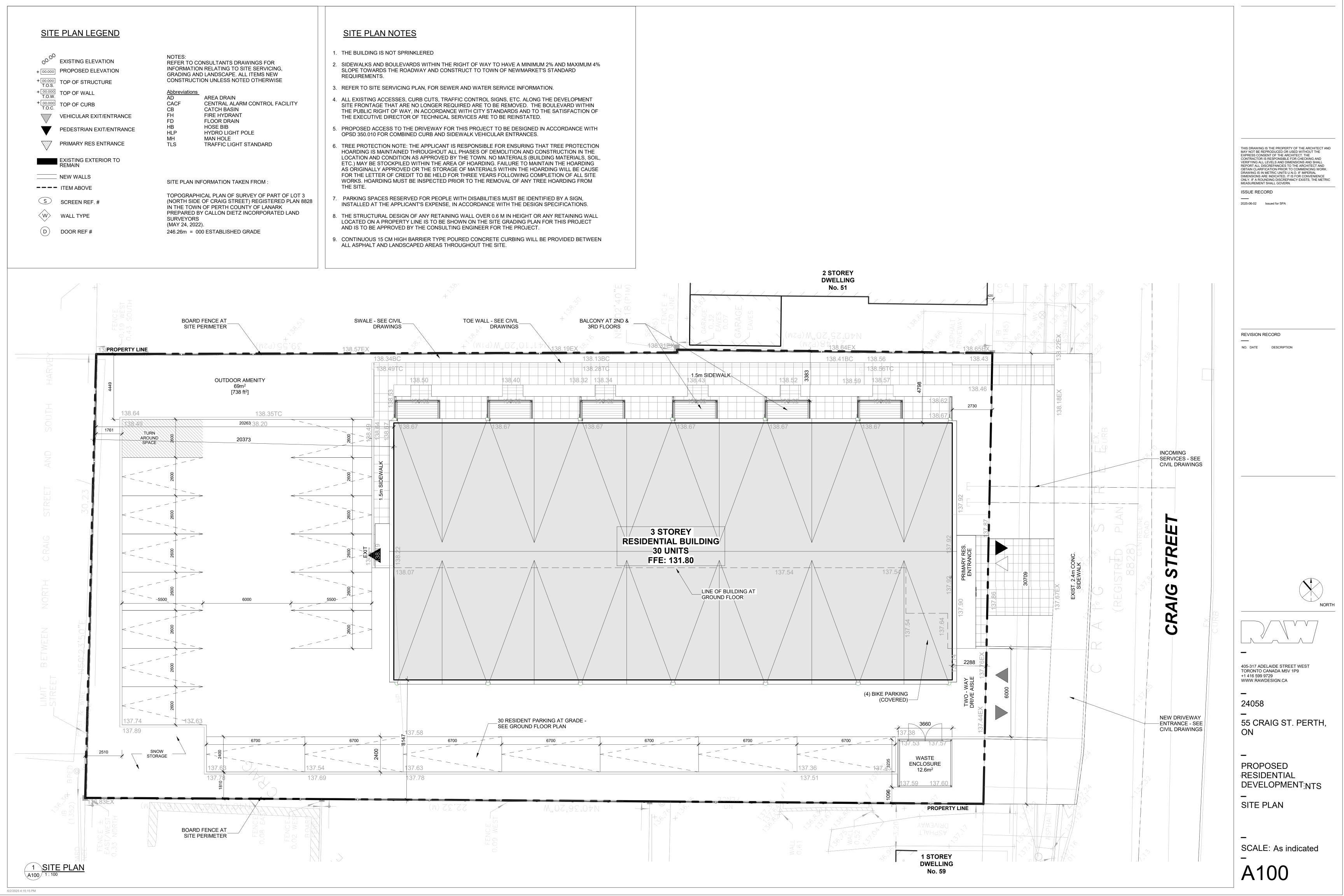
RENDERINGS

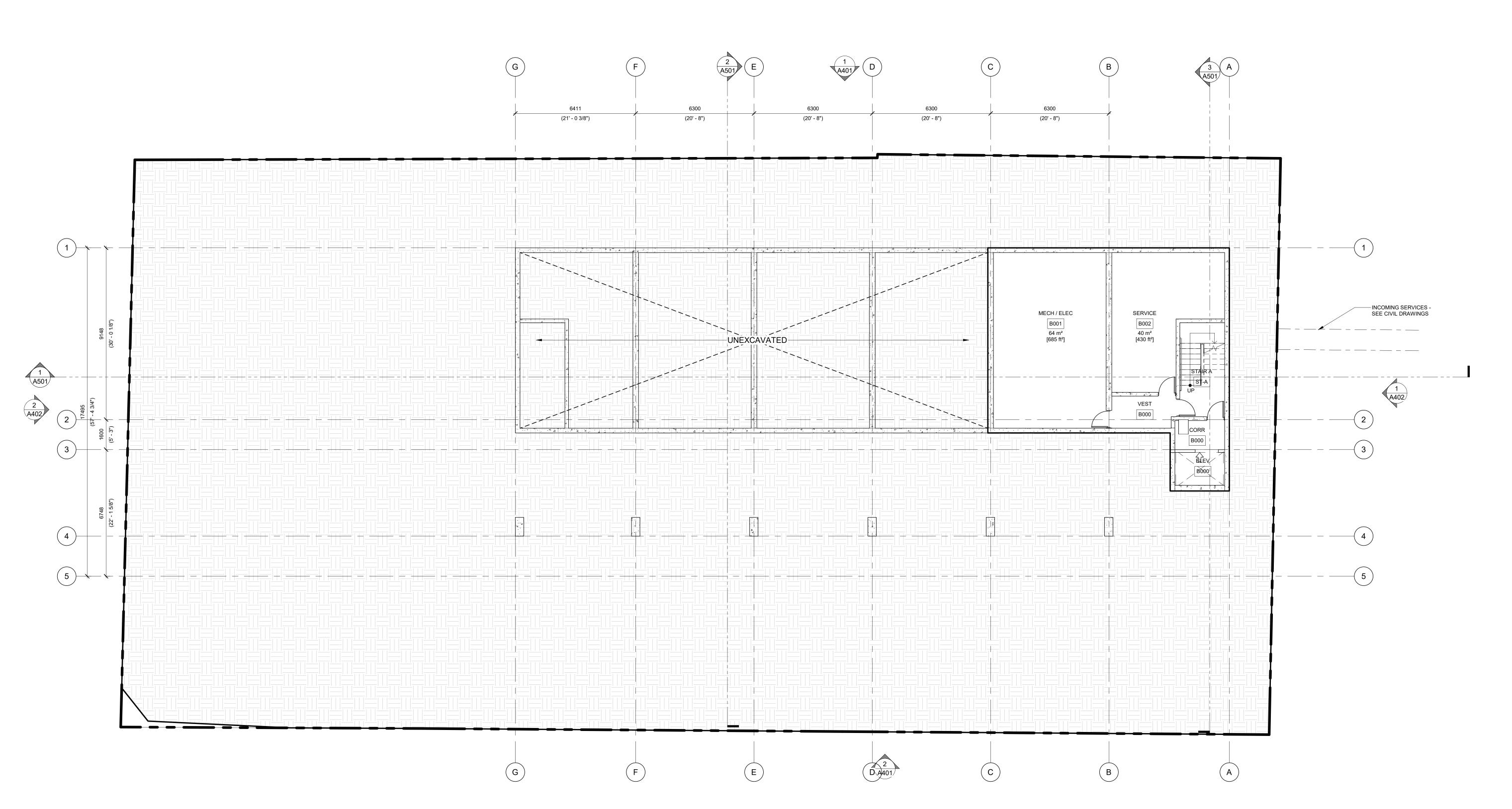
SCALE:

A003



4 EAST PERSPECTIVE A003 1:1





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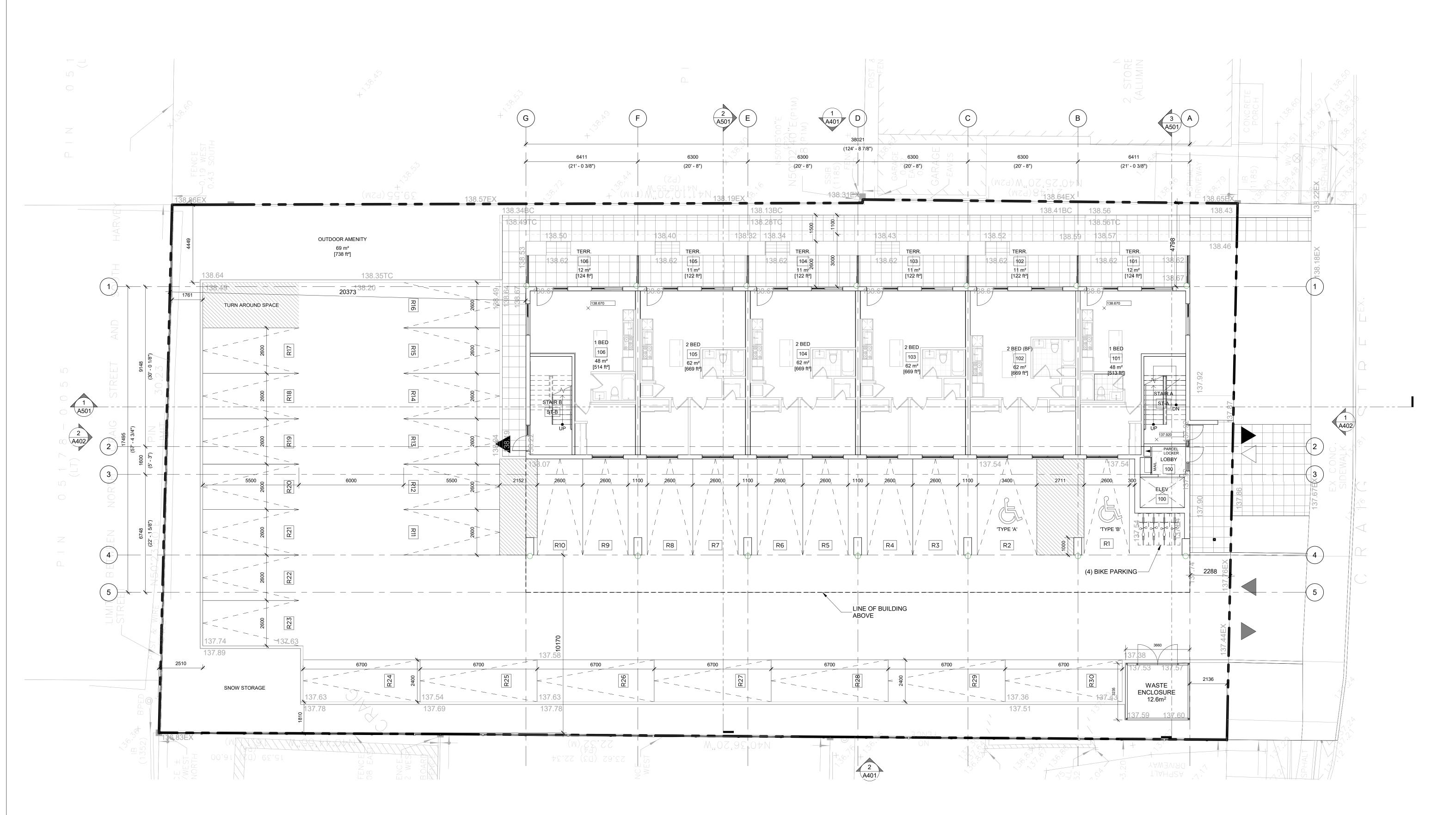
24058

55 CRAIG ST. PERTH, ON

PROPOSED
RESIDENTIAL
DEVELOPMENT:NTS

BASEMENT PLAN

SCALE: 1:100



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2025-06-02 Issued for SPA

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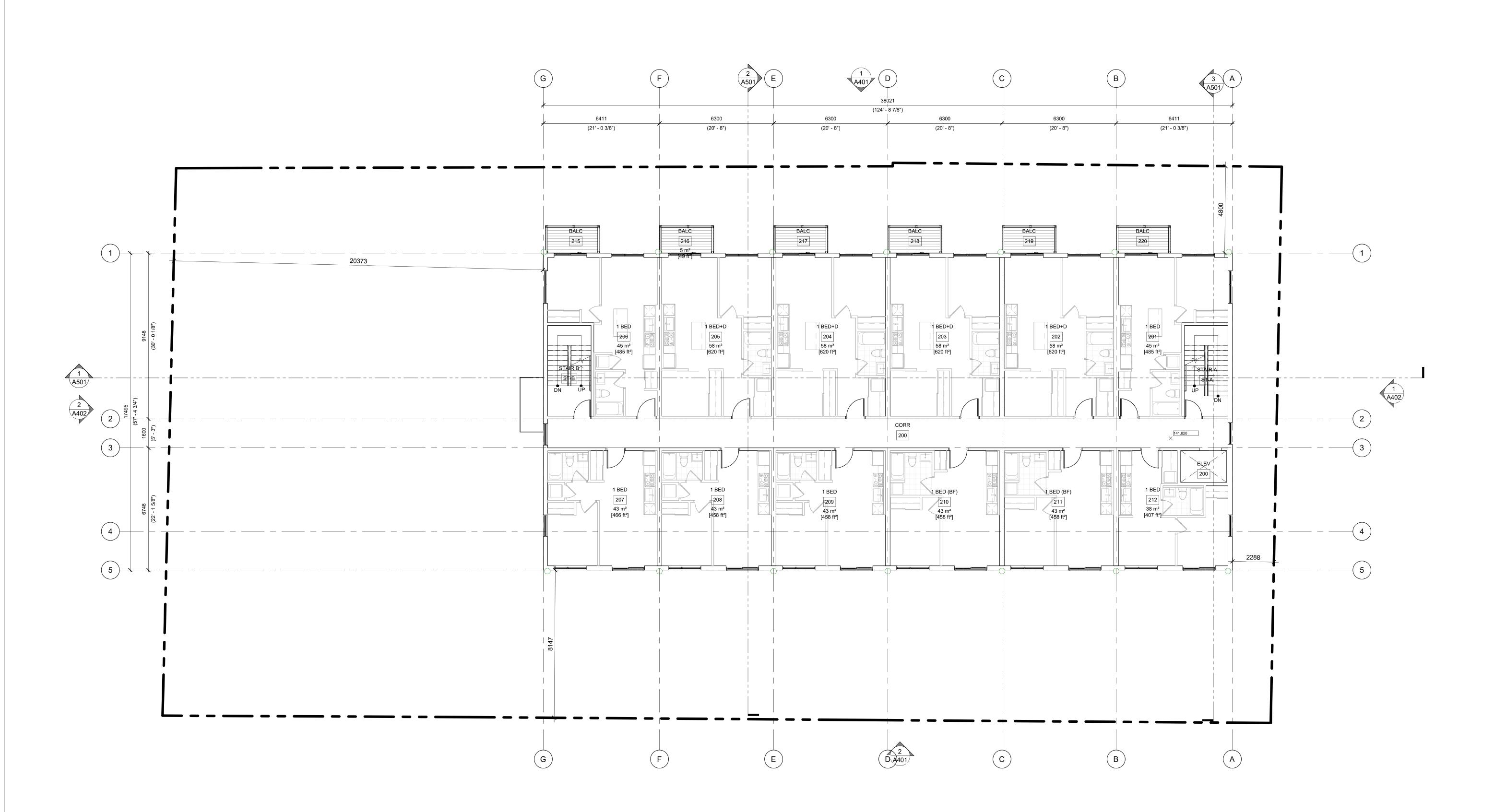
24058

55 CRAIG ST. PERTH, ON

PROPOSED RESIDENTIAL DEVELOPMENT:NTS

GROUND FLOOR PLAN

SCALE: 1:100



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55 CRAIG ST. PERTH, ON

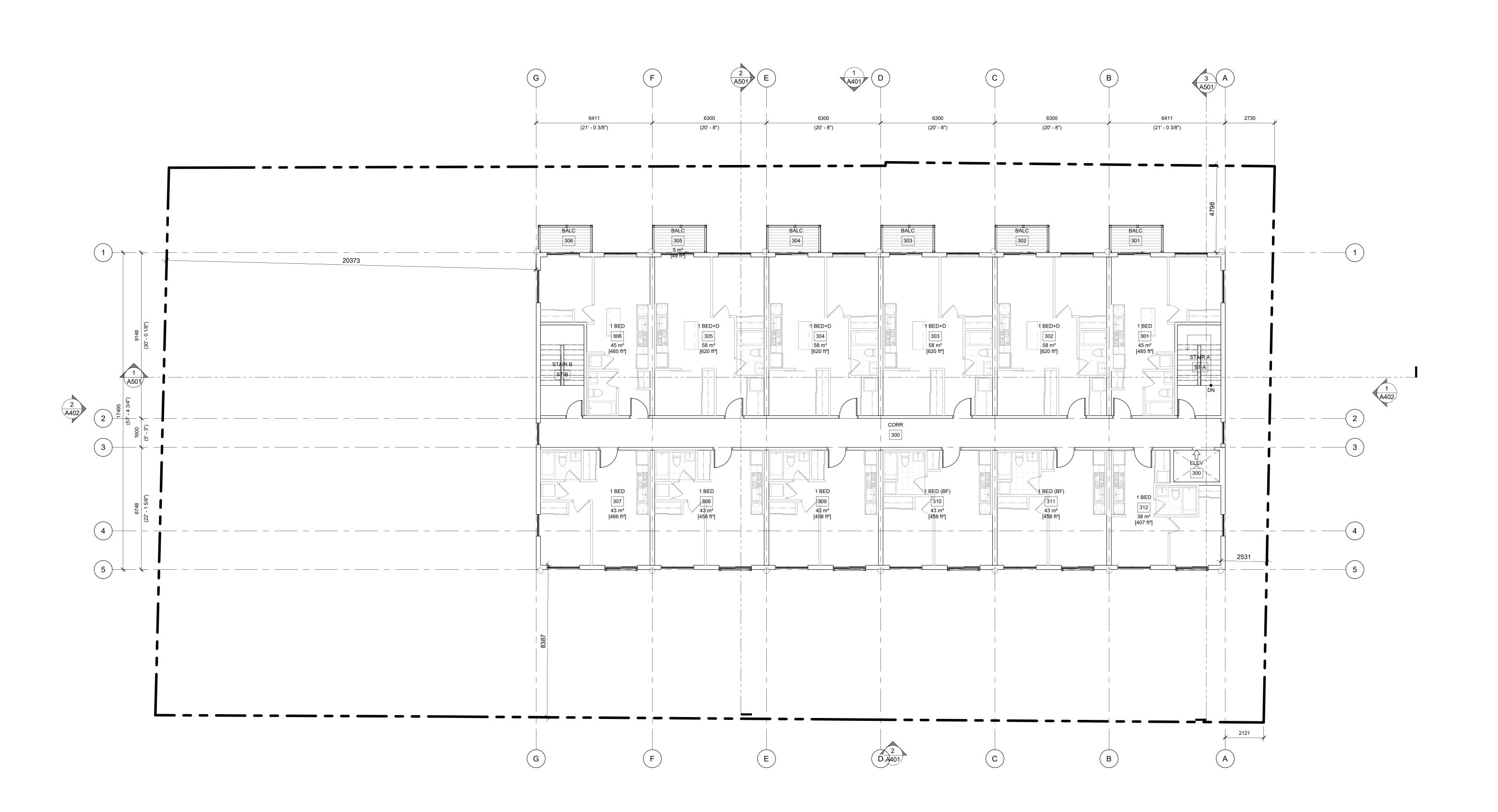
PROPOSED
RESIDENTIAL
DEVELOPMENT:NTS

2ND FLOOR PLAN

-SCALE: 1:100

-A202

6/2/2025 4:16:02 PM



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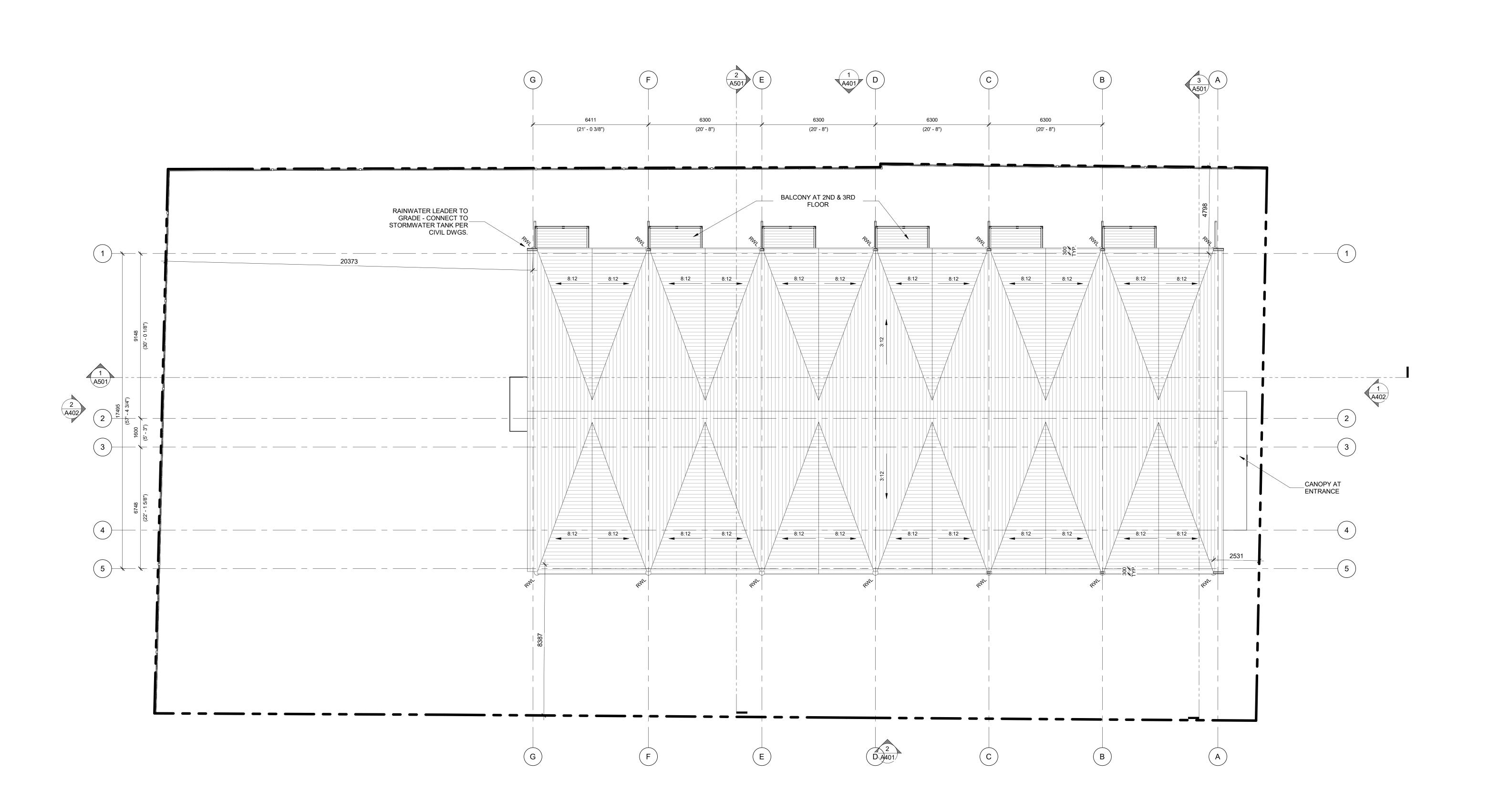
24058

55 CRAIG ST. PERTH, ON

PROPOSED
RESIDENTIAL
DEVELOPMENT:NTS

3RD FLOOR PLAN

SCALE: 1:100



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NORTH

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2405

55 CRAIG ST. PERTH,

PROPOSED
RESIDENTIAL
DEVELOPMENT:NTS

ROOF PLAN

SCALE: 1:100



MATERIAL LEGEND

ARCHITECTURAL SIDING -BOARD AND BATTEN - SAGE GREEN

ARCHITECTURAL SIDING -WOOD TONE

3 ARCHITECTURAL SIDING - CHARCOAL

CHARCOAL

4 STANDING SEAM METAL ROOF -

PREFINISHED METAL FASCIA / FLASHING / WINDOW FRAME - CHARCOAL

CLEAR GLAZING

METAL RAILING SYSTEM

WOOD PRIVACY SCREEN

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ISSUE RECORD

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REVISION RECORD

NO. DATE DESCRIPTION

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24058

_ 55 CRAIG ST. PERTH,

– PROPOSED

DEVELOPMENT:NTS

ELEVATIONS

RESIDENTIAL

SCALE: 1:100

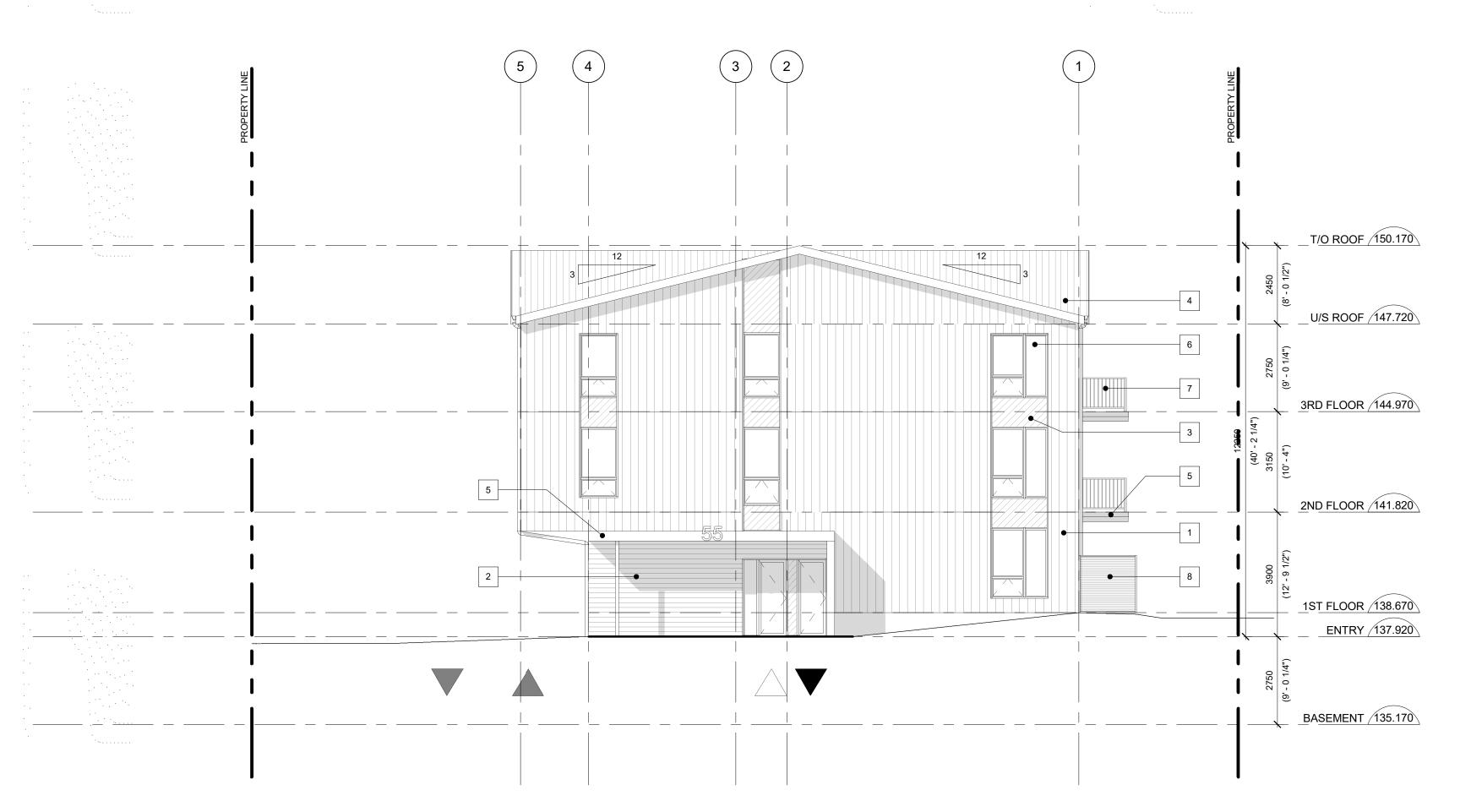
A401

1 NORTH ELEVATION 1:100

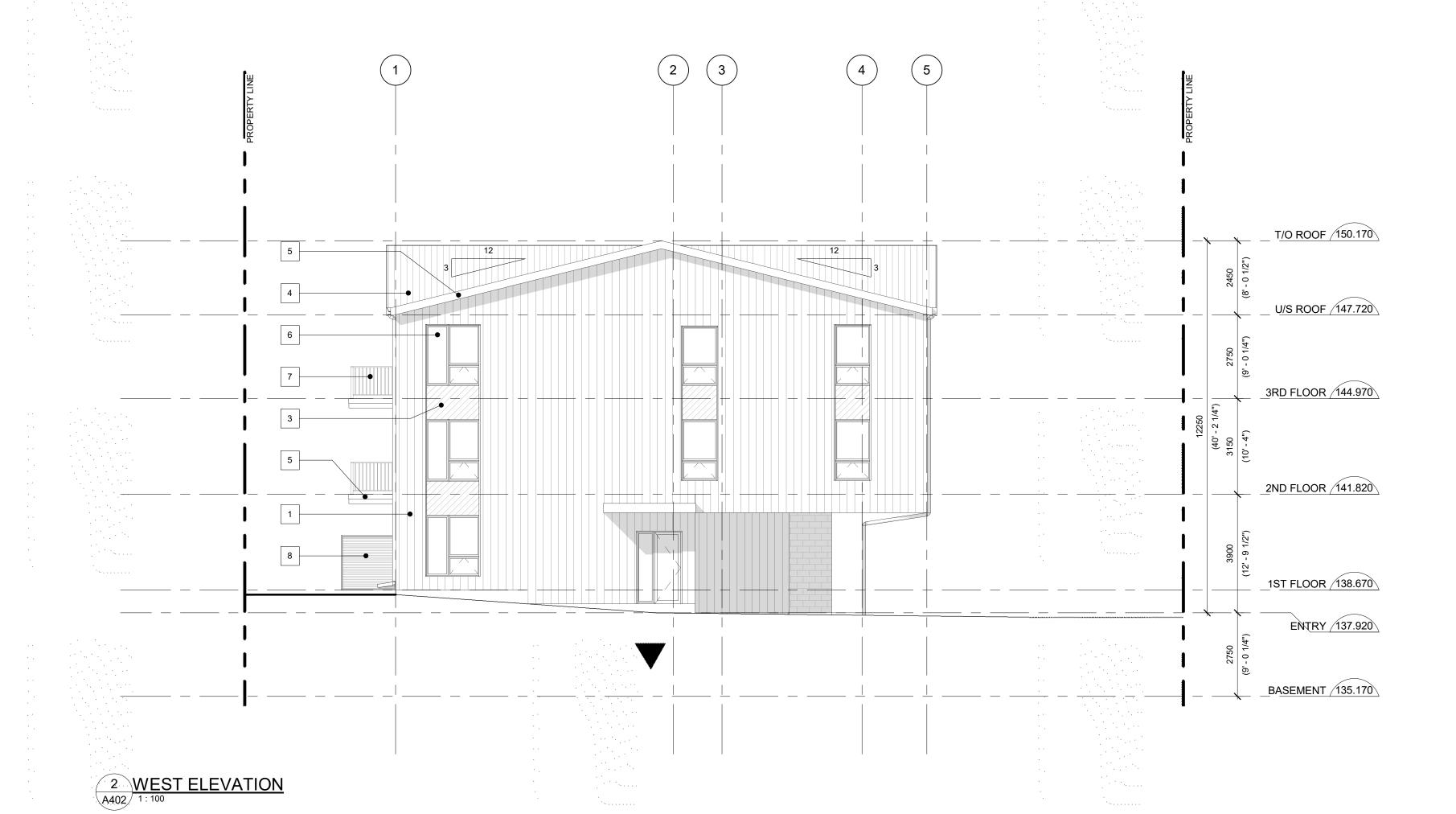


2 SOUTH ELEVATION 1:100

6/2/2025 4:16:29 PM



1 EAST ELEVATION



MATERIAL LEGEND

- 1 ARCHITECTURAL SIDING -BOARD AND BATTEN - SAGE GREEN
- 2 ARCHITECTURAL SIDING WOOD TONE
- 3 ARCHITECTURAL SIDING CHARCOAL
- 4 STANDING SEAM METAL ROOF -
- 5 PREFINISHED METAL FASCIA / FLASHING / WINDOW FRAME CHARCOAL
- 6 CLEAR GLAZING

CHARCOAL

- METAL RAILING SYSTEM
- 8 WOOD PRIVACY SCREEN

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REVISION RECORD

NO. DATE DESCRIPTION

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24058

55 CRAIG ST. PERTH, ON

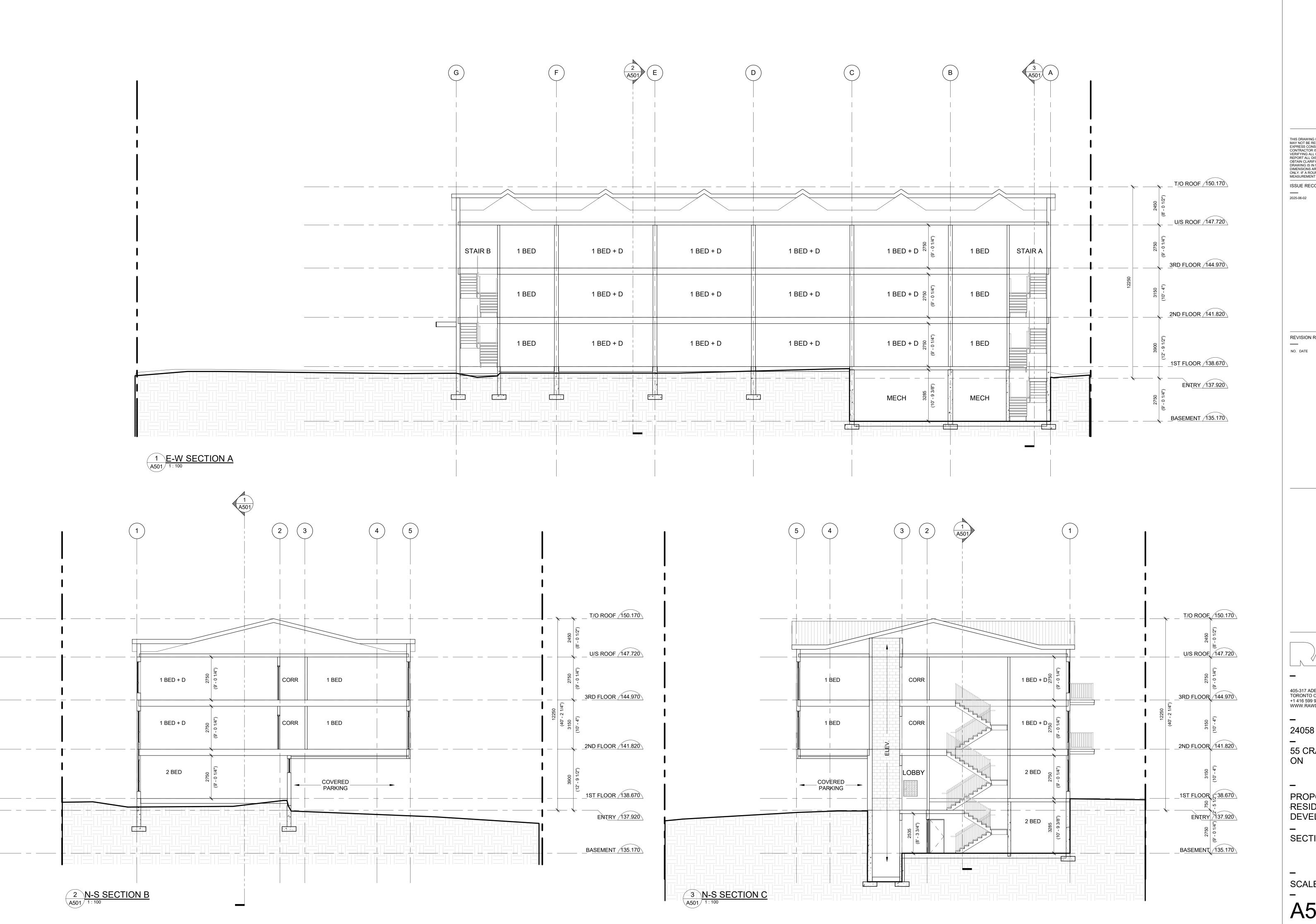
PROPOSED
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DEVELOPMENTINTS

ELEVATIONS

SCALE: 1:100

A402

6/2/2025 4:16:41 PM



6/2/2025 4:16:49 PM

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ISSUE RECORD

2025-06-02 Issued for SPA

REVISION RECORD

NO. DATE DESCRIPTION

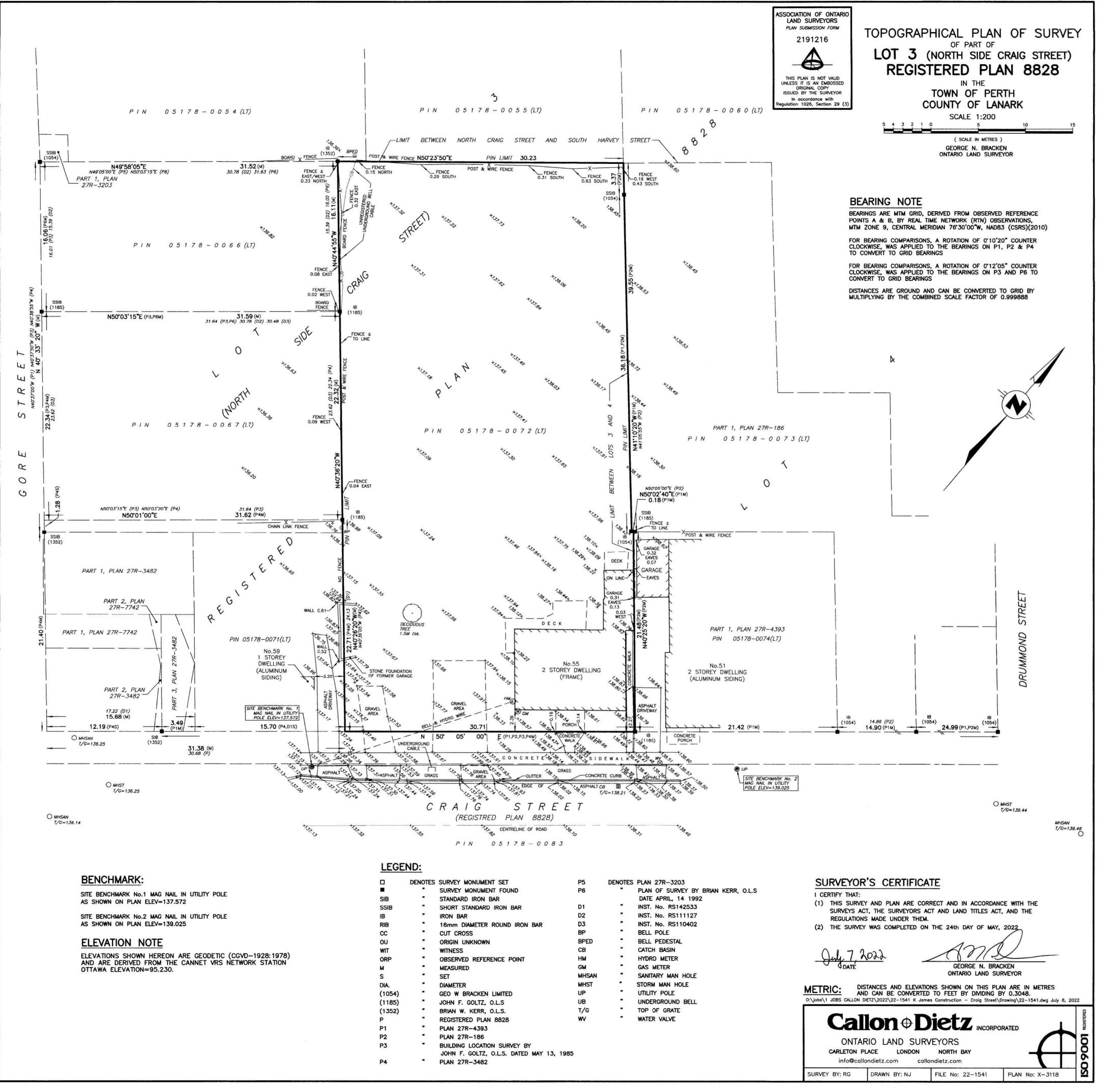
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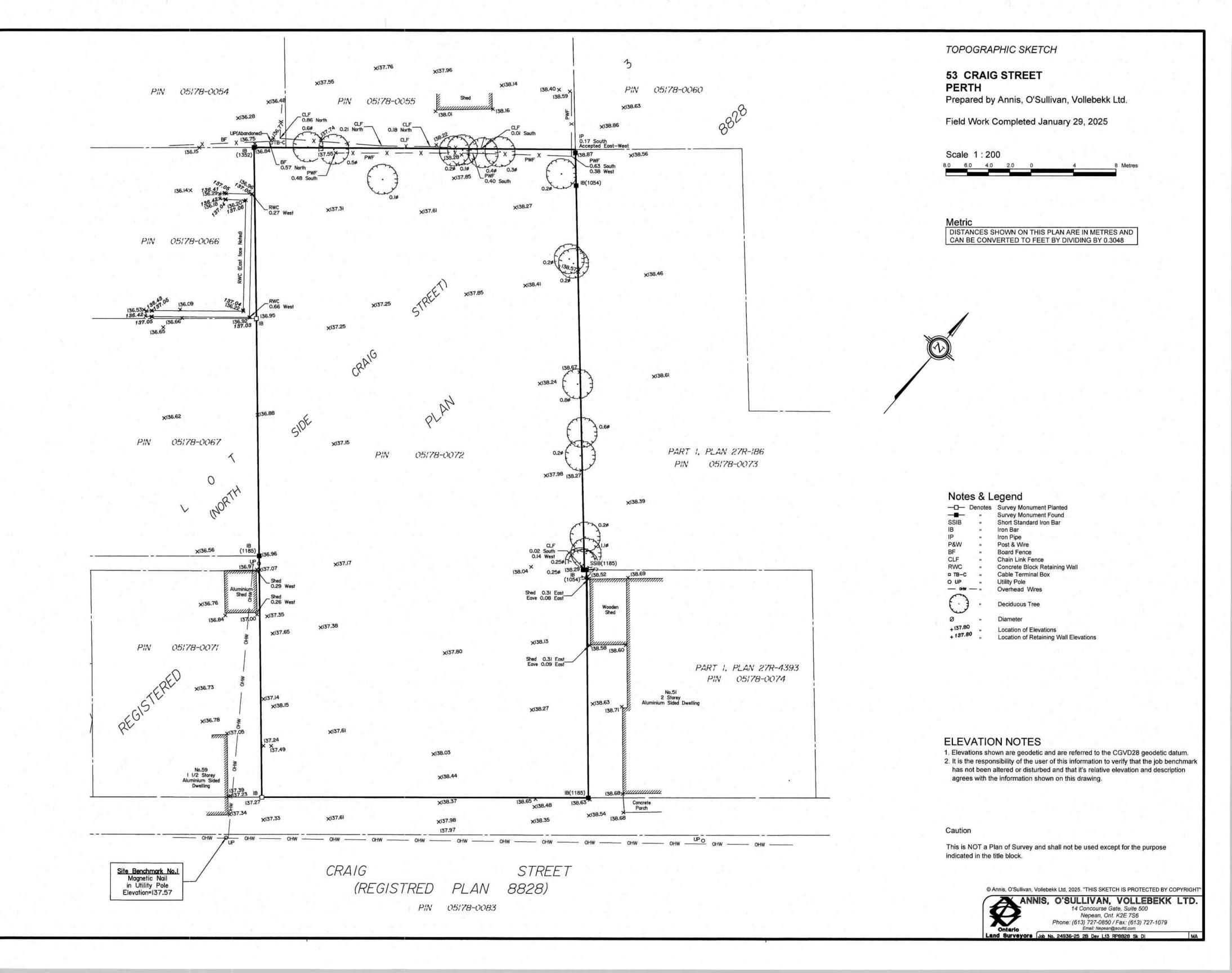
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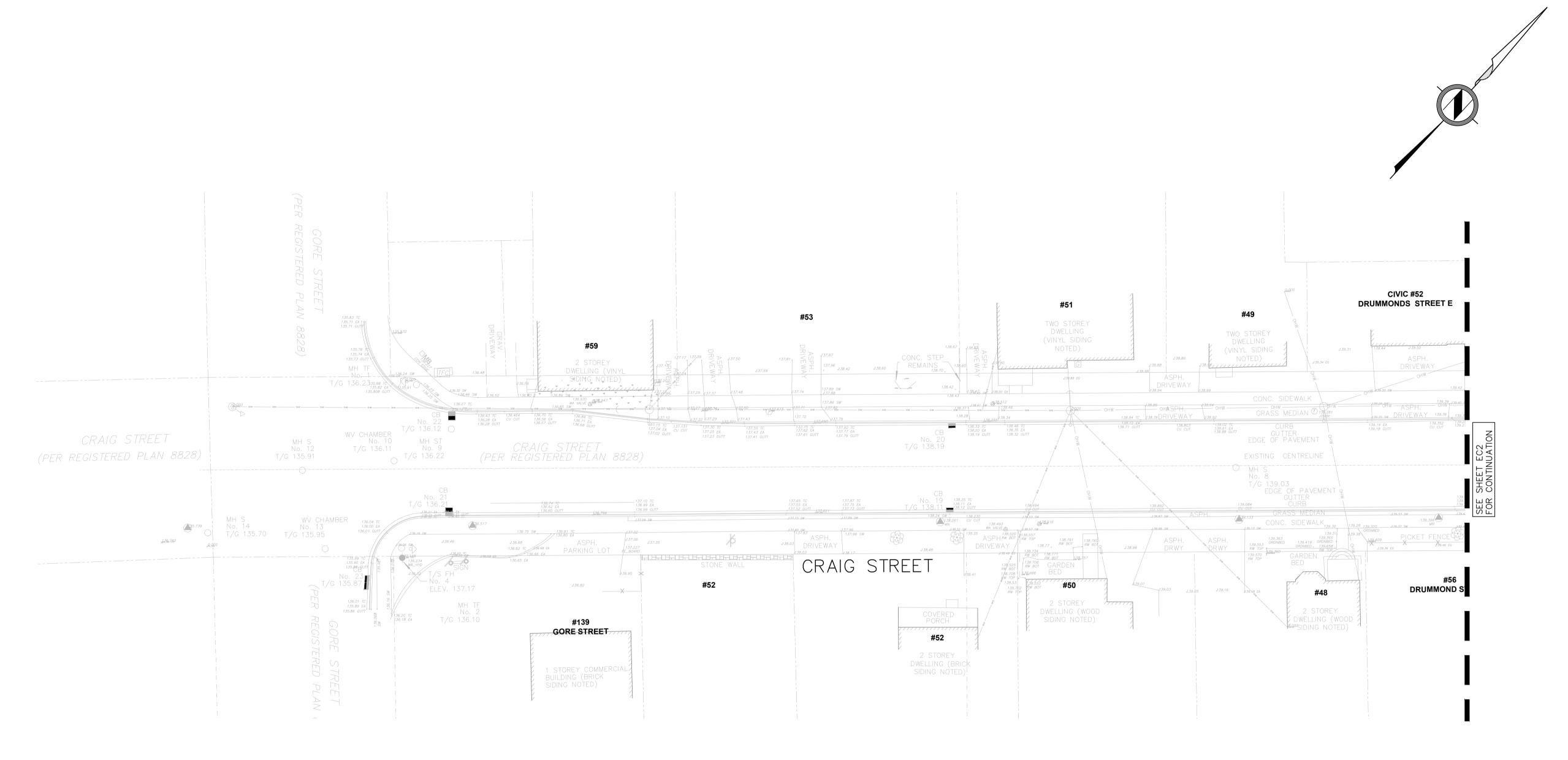
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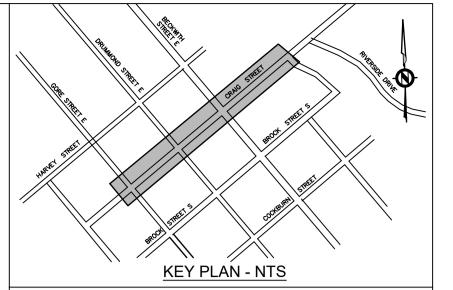
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SCALE: 1:100



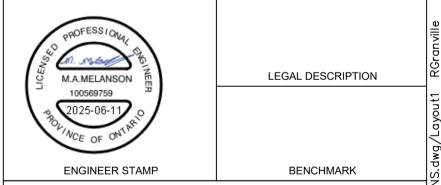






PROPERTY LINE	
EXISITING EDGE OF ASPHALT	
EXISTING SANITARY	s
EXISTING WATERMAIN	
EXISTING STORM	— D — — — —
PROPOSED STORM	— D— — —
PROPOSED WATERMAIN	— W—— – ——
PROPOSED SANITARY	s
PROPOSED EDGE OF ASPHALT	111
PROPOSED SWALE	
EXISTING GROUND CONTOUR	46.5—
EXISTING/PROPOSED ELEVATION	× 252.76 /×252.76
TOP/BOTTOM OF WALL ELEVATION	×274.78TW/BW
GRADE	2.0%
EXISTING/PROPOSED CATCH BASIN	riangledown / lacktriangledown
EXISTING/PROPOSED CATCH BASIN M	IANHOLE 🛛 / 🗖
EXISTING/PROPOSED MANHOLE	0/•
EXISTING/PROPOSED FIRE HYDRANT	-⊕- / ◆ Н
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3	03/07/2025	NDER	R.G	J.S	
2	02/28/2025	ISSUED FOR 90% DETA	AILED DESIGN	R.G	J.S
			== ===		



ISSUED FOR 60% DETAILED DESIGN

DESCRIPTION

R.G J.S

BY APP



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1000 Innovation Drive Suite 500, Ottawa, O.N. Canada K2K 3E7
Tel: (613) 809-3889, Fax: (416) 644-1889, Email: ottawa@aplinmartin.com

CLIENT

1 02/18/2025

REV DATE

THE TOWN OF PERTH

PROJECT

CRAIG STREET RECONSTRUCTION

DRAWING TITLE

EXISTING CONDITIONS (SHEET 1 OF 4)

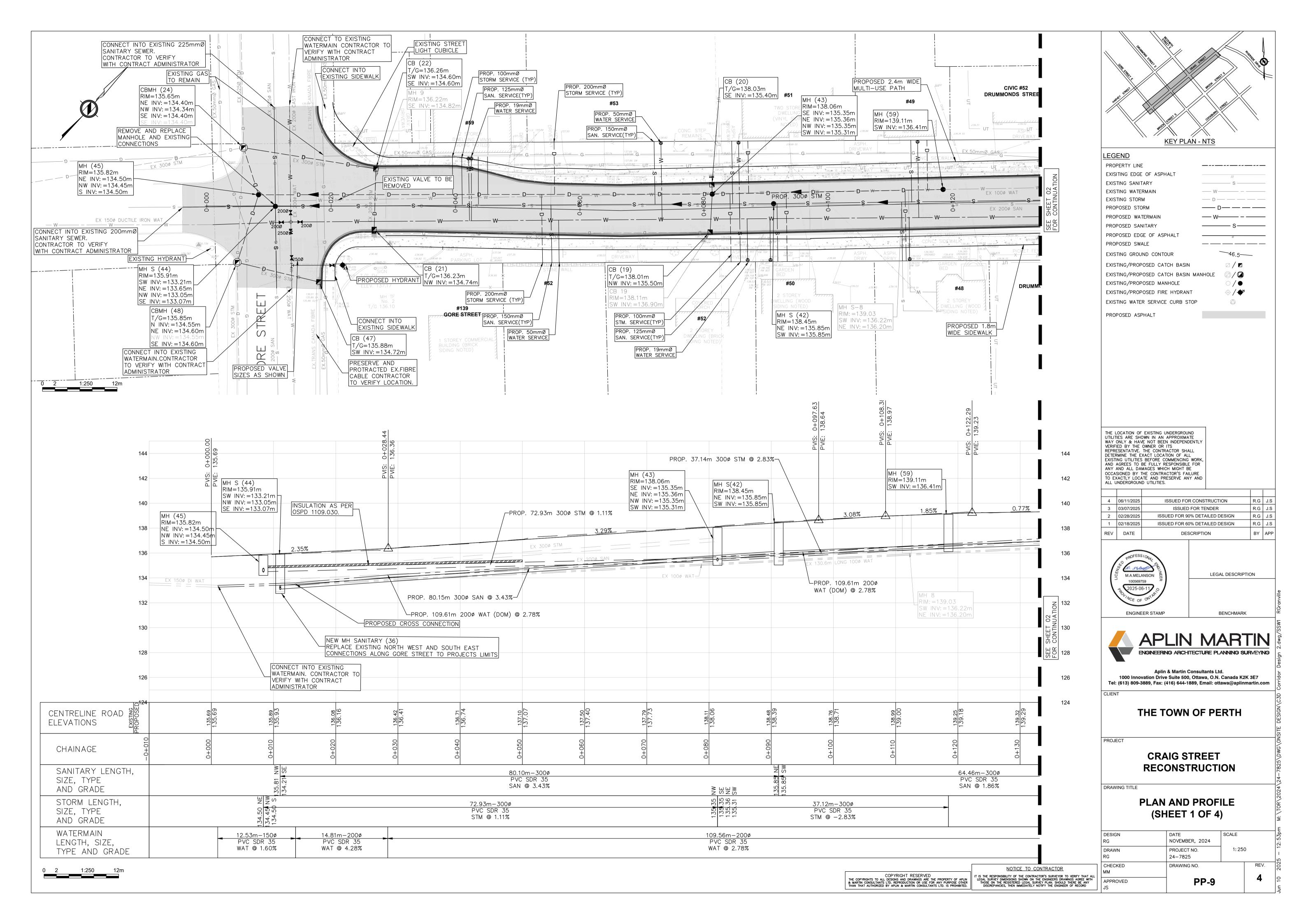
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DESIGN RG	DATE NOVEMBER, 2024	SCALE		1. 5: 16pm
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APPROVED JS	EC-1		4	Jun 05

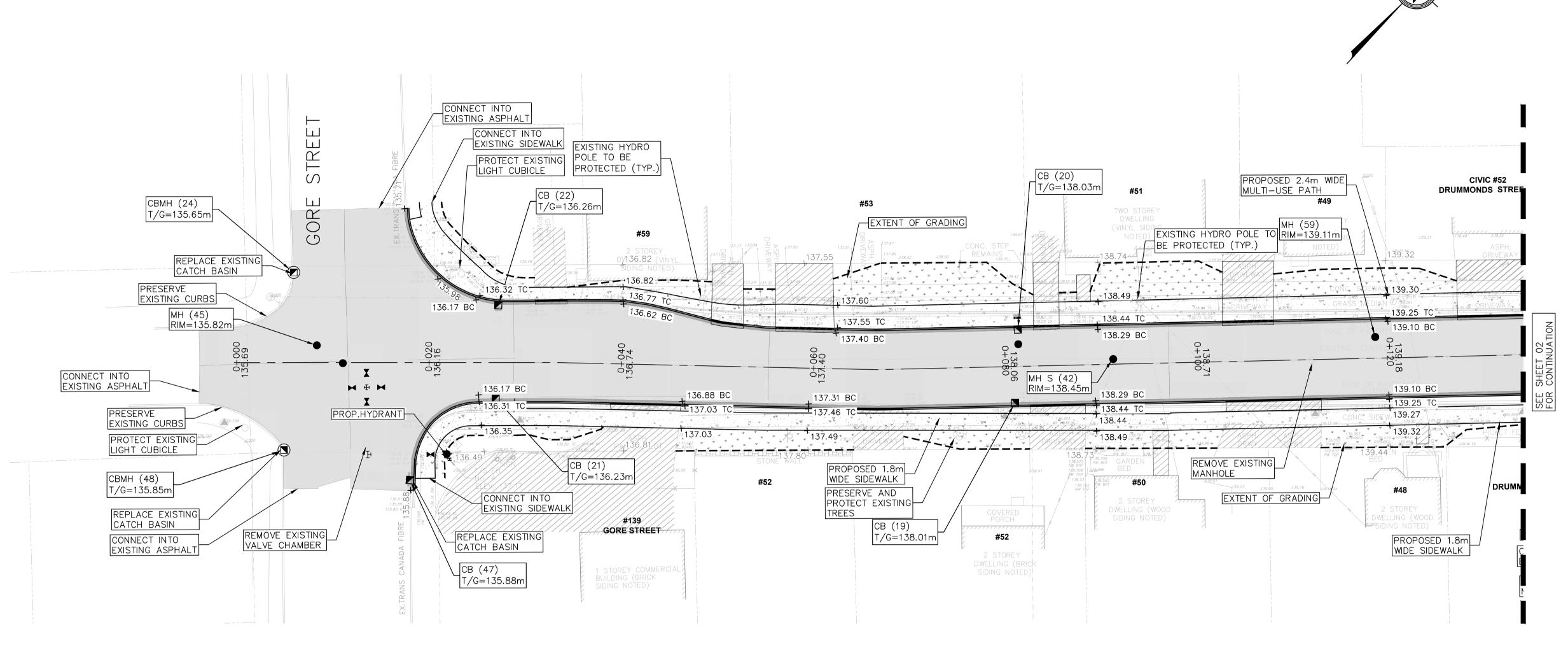
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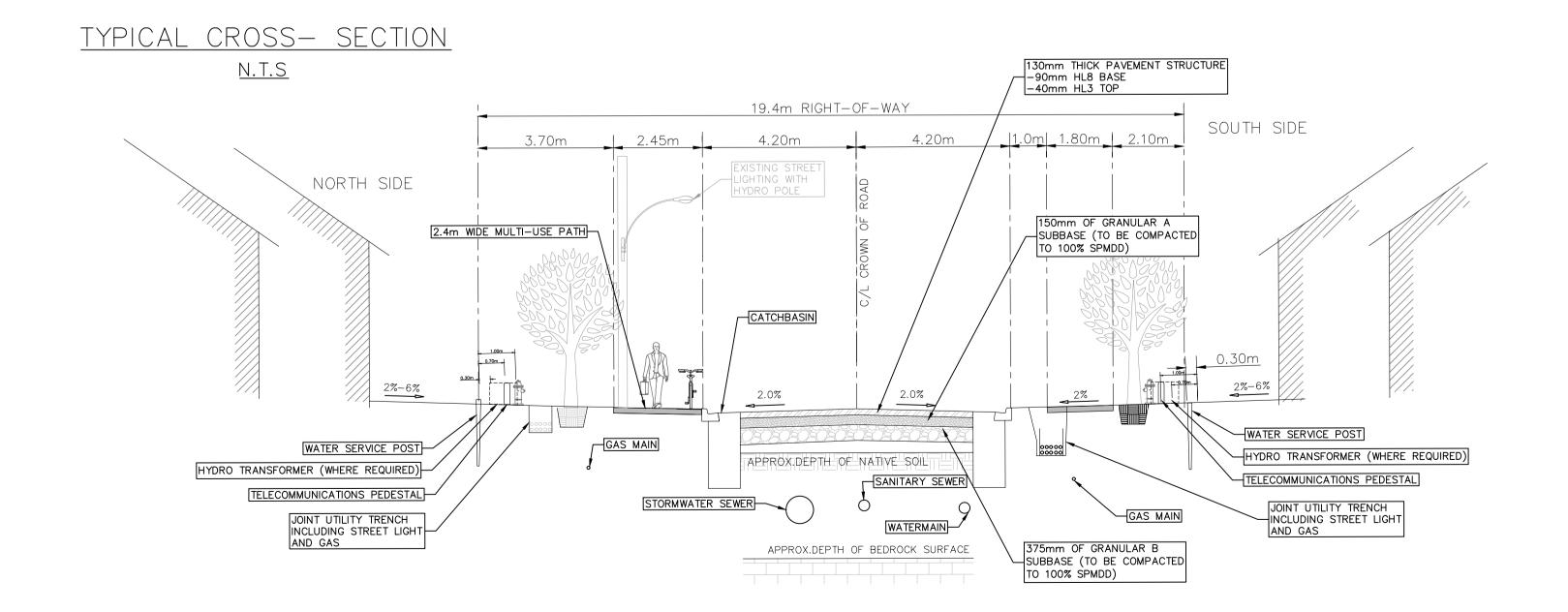
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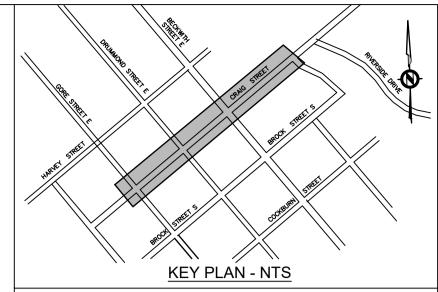
NOTICE TO CONTRACTOR

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LEGEND	
PROPERTY LINE	
EXISITING EDGE OF ASPHALT	
EXISTING SANITARY	
EXISTING WATERMAIN	W
EXISTING STORM	— D — — — —
PROPOSED STORM	$-\!\!\!-\!\!\!\!-\!\!\!\!-\!\!\!\!-\!\!\!\!-\!\!\!\!-\!\!\!\!-\!\!$
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PROPOSED SWALE	
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TOP/BOTTOM OF WALL ELEVATION	×274.78TW/BW
GRADE	2.0%
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EXISTING/PROPOSED FIRE HYDRANT	- -
PROPOSED ASPHALT	
REGRADED GRASSED EXTENT	V
PROPOSED CURB	
PROPOSED DRIVEWAY TO BE REGRADED	
PROPOSED SIDEWALK/ MULTI-USE PATHWAY	
THE LOCATION OF EXISTING UNDERGROUND UTILITIES ARE SHOWN IN AN APPROXIMATE WAY ONLY & HAVE NOT BEEN INDEPENDEN VERIFIED BY THE OWNER OR ITS REPRESENTATIVE. THE CONTRACTOR SHALL DETERMINE THE EXACT LOCATION OF ALL EXISTING UTILITIES BEFORE COMMENCING WAND AGREES TO BE FULLY RESPONSIBLE FANY AND ALL DAMAGES WHICH MIGHT BE OCCASIONED BY THE CONTRACTOR'S FAILUITO EXACTLY LOCATE AND PRESERVE ANY ALL UNDERGROUND UTILITIES.	ORK, OR OR

4	06/11/2025	ISSUED FOR CONSTRUCTION	R.G	J.S
3	03/07/2025	ISSUED FOR TENDER	R.G	J.S
2	02/28/2025	ISSUED FOR 90% DETAILED DESIGN	R.G	J.S
1	02/18/2025	ISSUED FOR 60% DETAILED DESIGN	R.G	J.S
REV	DATE	DESCRIPTION	BY	APP



LEGAL DESCRIPTION

BENCHMARK

GINEER STAMP



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CLIENT

THE TOWN OF PERTH

PROJECT

CRAIG STREET RECONSTRUCTION

DRAWING TITLE

GRADING PLAN (SHEET 1 OF 4)

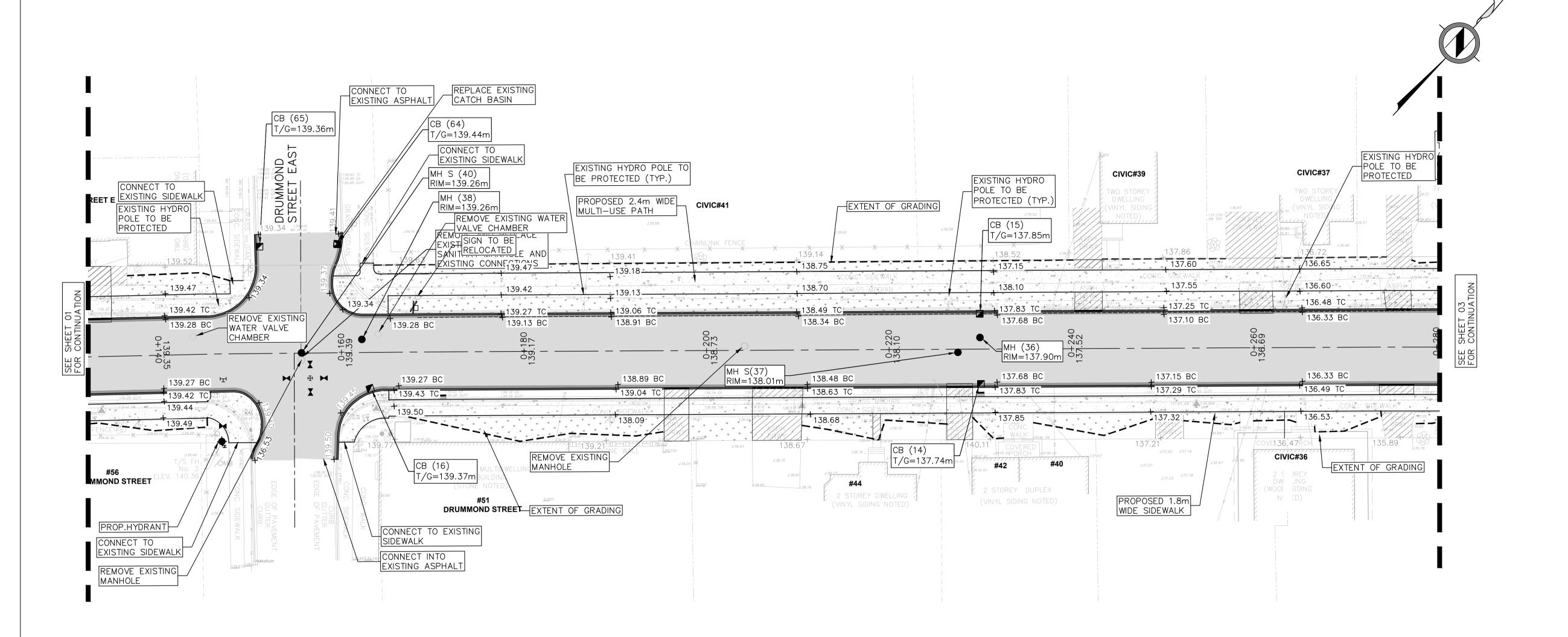
APPROVED JS	GR-1		4
CHECKED MM	DRAWING NO.		REV.
DRAWN RG	PROJECT NO. 24-7825	1: 250	0
DESIGN RG	DATE NOVEMBER, 2024	SCALE	

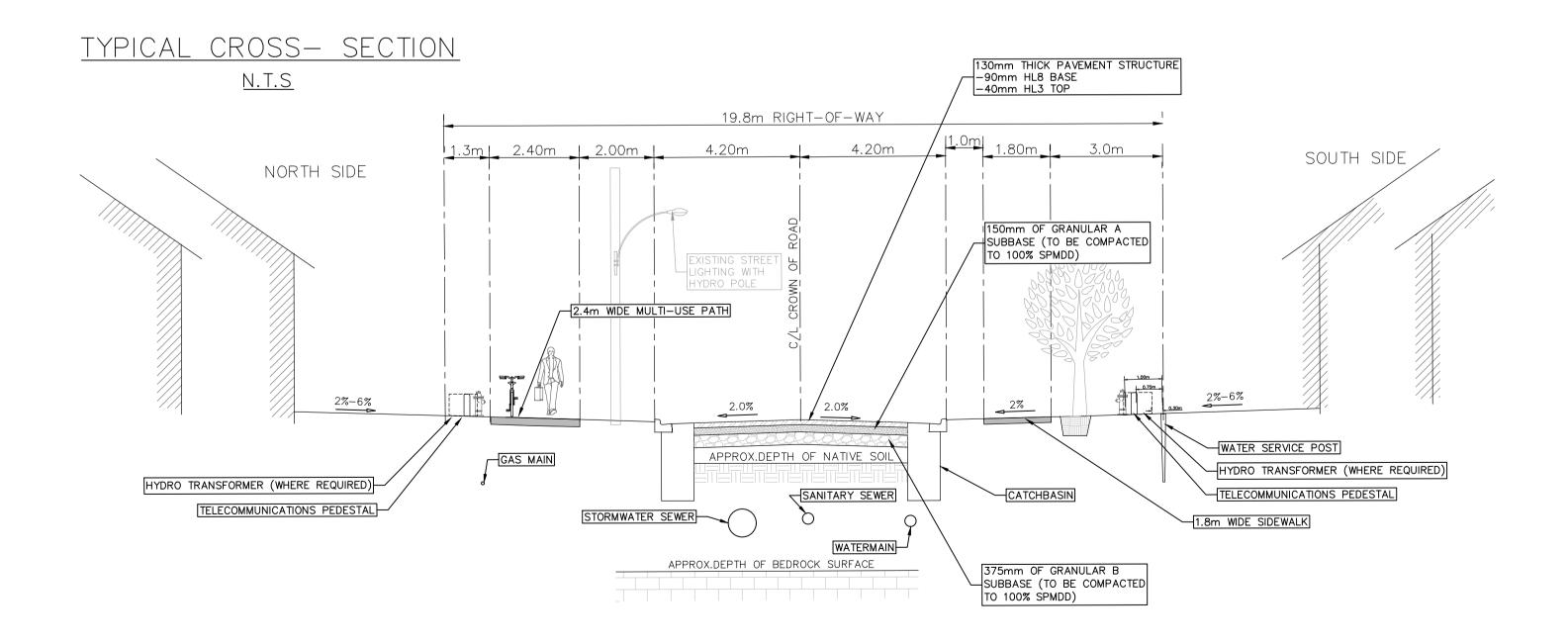
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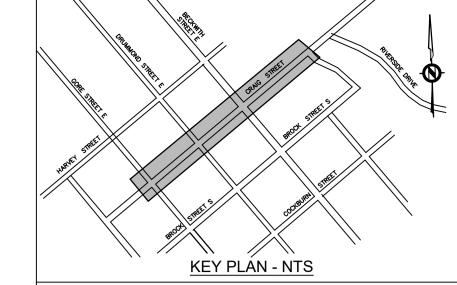
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DISCREPANCIES, THEN IMMEDIATELY NOTIFY THE ENGINEER OF RECORD







<u>LEGEND</u>	
PROPERTY LINE	
EXISITING EDGE OF ASPHALT	
EXISTING SANITARY	S
EXISTING WATERMAIN	W
EXISTING STORM	$-\!-\!\!\!\!\!-\!\!\!\!\!-\!\!\!\!\!-\!\!\!\!\!-\!\!\!\!\!-\!\!\!\!\!-\!\!\!\!$
PROPOSED STORM	— D— — —
PROPOSED WATERMAIN	— W—— – —
PROPOSED SANITARY	s
PROPOSED EDGE OF ASPHALT	
PROPOSED SWALE	
EXISTING GROUND CONTOUR	46.5
EXISTING/PROPOSED ELEVATION	× 252.76 /×252.7 0
TOP/BOTTOM OF WALL ELEVATION	×274.78TW/BW
GRADE	2.0%
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EXISTING/PROPOSED MANHOLE	0/•
EXISTING/PROPOSED FIRE HYDRANT	
PROPOSED ASPHALT	
	V V V V
REGRADED GRASSED EXTENT	Ψ Ψ Ψ Ψ Ψ

THE LOCATION OF EXISTING UNDERGROUND UTILITIES ARE SHOWN IN AN APPROXIMATE
WAY ONLY & HAVE NOT BEEN INDEPENDENTLY
VERIFIED BY THE OWNER OR ITS
REPRESENTATIVE. THE CONTRACTOR SHALL
DETERMINE THE EXACT LOCATION OF ALL
EXISTING UTILITIES BEFORE COMMENCING WORK
AND AGREES TO BE FULLY RESPONSIBLE FOR
ANY AND ALL DAMAGES WHICH MIGHT BE
OCCASIONED BY THE CONTRACTOR'S FAILURE
TO EXACTLY LOCATE AND PRESERVE ANY AND
ALL UNDERGROUND UTILITIES.

PROPOSED DRIVEWAY

PROPOSED SIDEWALK/

MULTI-USE PATHWAY

TO BE REGRADED

4	06/11/2025	ISSUED FOR CONSTRUCTION	R.G	J.S
3	03/07/2025	ISSUED FOR TENDER	R.G	J.S
2	02/28/2025	ISSUED FOR 90% DETAILED DESIGN	R.G	J.S
1	02/18/2025	ISSUED FOR 60% DETAILED DESIGN	R.G	J.S
REV	DATE	DESCRIPTION	BY	APP



LEGAL DESCRIPTION

BENCHMARK



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THE TOWN OF PERTH

PROJECT

CRAIG STREET RECONSTRUCTION

DRAWING TITLE

GRADING PLAN (SHEET 2 OF 4)

	DESIGN RG	DATE NOVEMBER, 2024	SCALE		: 05pm
	DRAWN RG	PROJECT NO. 24-7825	1: 25	0	5 – 1
	CHECKED MM	DRAWING NO.		REV.	202
•	APPROVED JS	GR-2		4	Jun 10

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Appendix B

Existing Conditions and Removals Plan (DWG. 24116-R1)

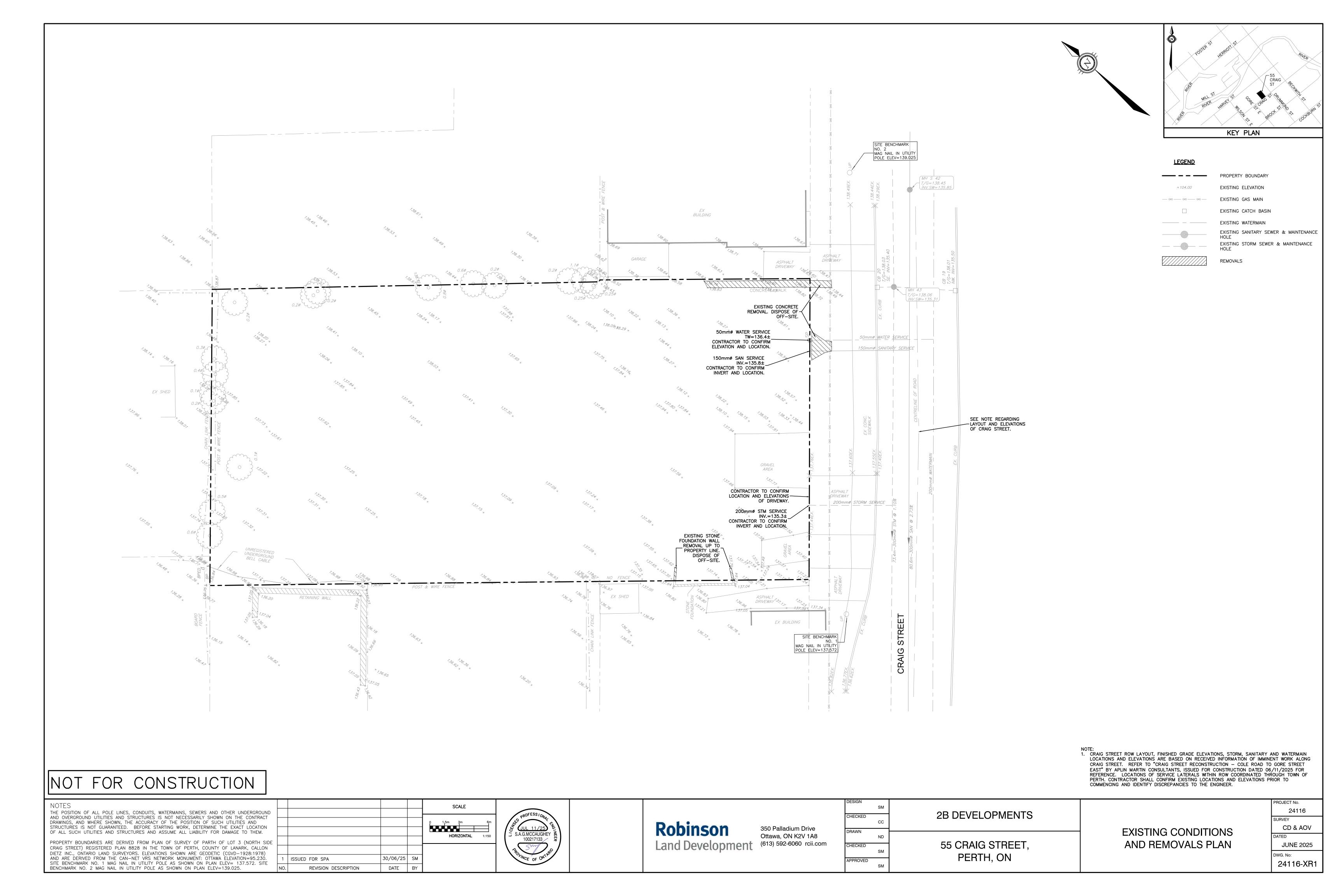
Servicing Plan (DWG. 24116-S1)

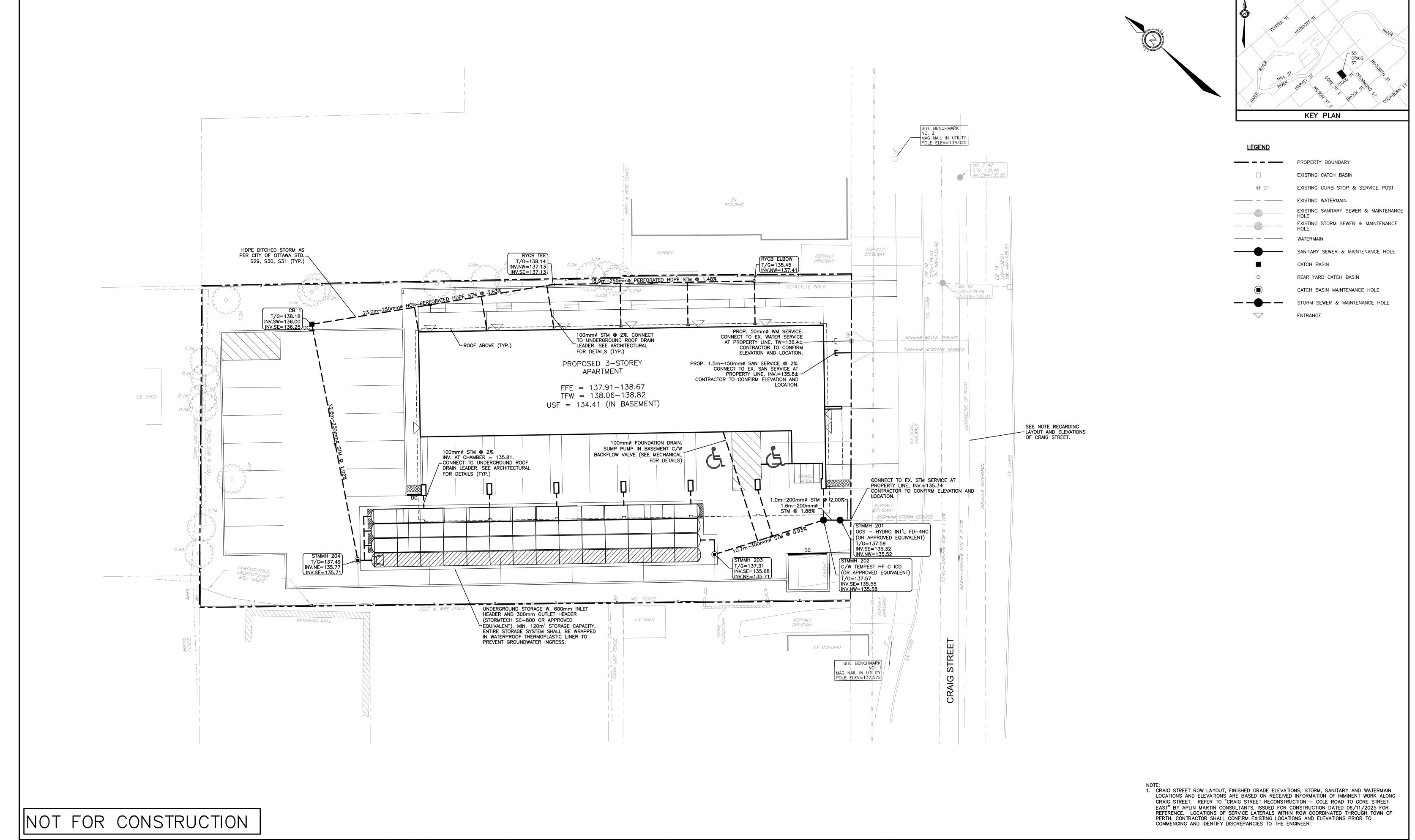
Grading Plan (DWG. 24116-GR1)

Erosion and Sediment Control Plan (DWG. 24116-ESC1)

Notes & Details (DWG. 24116-N1)

Storm Drainage Area Plan (DWG. 24116-STM1)





NOTES
THE POSITION OF ALL POLE LINES, CONDUITS, WATERMAINS, SEWERS AND OTHER UNDERGROUND AND OVERGROUND UTILITIES AND STRUCTURES IS NOT NECESSARILY SHOWN ON THE CONTRACT DRAWINGS, AND WHERE SHOWN, THE ACCURACY OF THE POSITION OF SUCH UTILITIES AND STRUCTURES IS NOT GUARANTEED. BEFORE STARTING WORK, DETERMINE THE EXACT LOCATION OF ALL SUCH UTILITIES AND STRUCTURES AND ASSUME ALL LIABILITY FOR DAMAGE TO THEM.

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				0 1.5m 3m 6m	
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				HOMEOWIAL 1.133	
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350 Palladium Drive Ottawa, ON K2V 1A8 (613) 592-6060 rcii.com

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2B DEVELOPMENTS

55 CRAIG STREET, PERTH, ON SITE SERVICING PLAN

PROJECT No.

24116

SURVEY

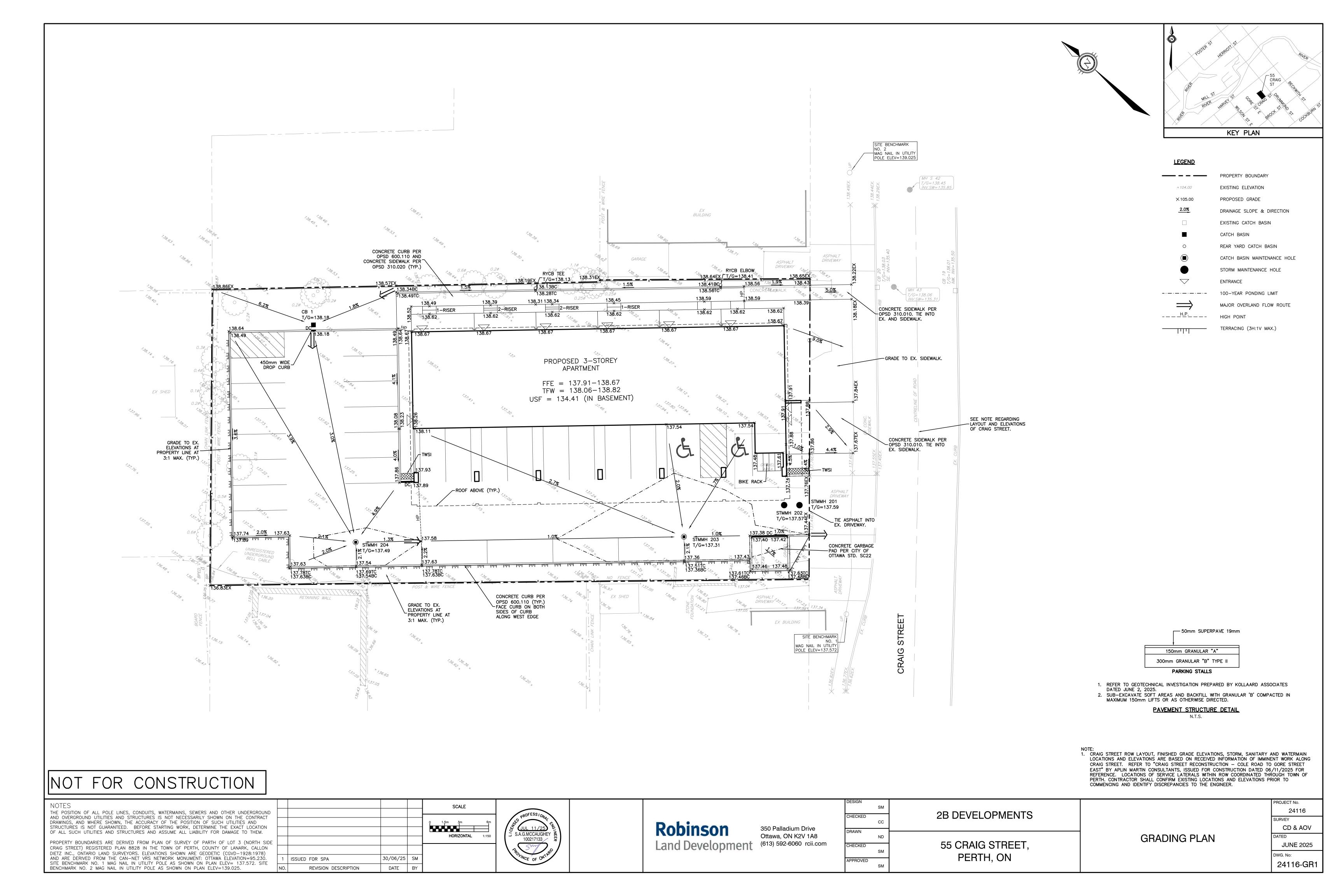
CD & AOV

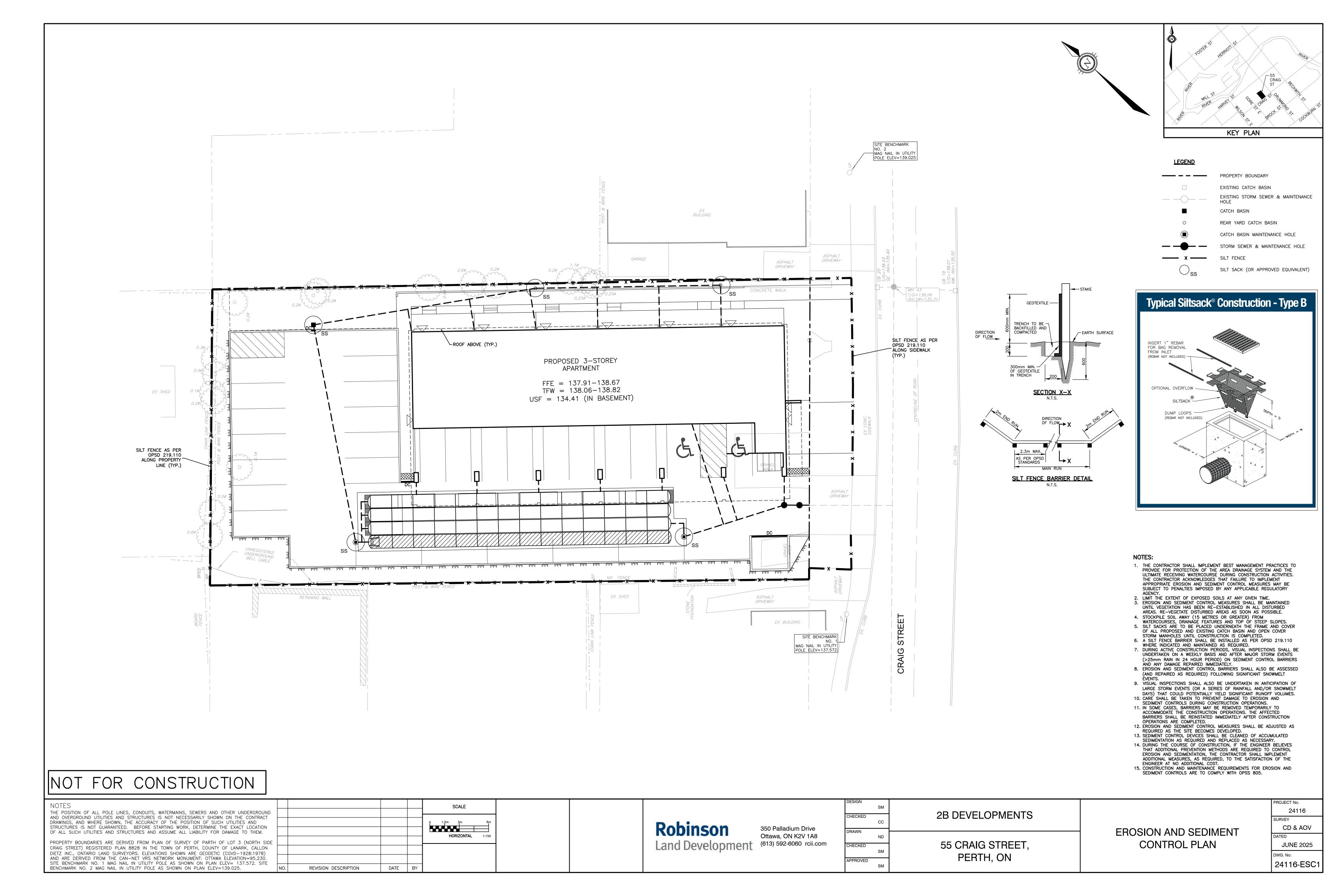
DATED

JUNE 2025

DWG. No:

24116-S1





GENERAL NOTES:

- 1. ALL WORKS AND MATERIALS SHALL CONFORM TO THE LATEST REVISIONS OF THE STANDARDS AND SPECIFICATIONS OF THE TOWN OF PERTH AND ONTARIO PROVINCIAL STANDARD DRAWINGS (OPSD) AND
- SPECIFICATIONS (OPSS), AS AMENDED BY THE TOWN OF PERTH.

 2. THE CONTRACTOR SHALL CONFIRM THE LOCATION OF ALL EXISTING UTILITIES WITHIN THE SITE AND ADJACENT WORK AREAS. THE CONTRACTOR SHALL BE RESPONSIBLE FOR PROTECTING ALL EXISTING UTILITIES TO THE SATISFACTION OF THE AUTHORITY HAVING JURISDICTION. THE CONTRACTOR SHALL BE RESPONSIBLE FOR REPAIR OR REPLACEMENT OF ANY SERVICES OR UTILITIES DISTURBED DURING
- CONSTRUCTION, TO THE SATISFACTION OF THE AUTHORITY HAVING JURISDICTION.

 3. ALL DIMENSIONS AND ELEVATIONS SHALL BE CHECKED AND VERIFIED IN THE FIELD BY THE CONTRACTOR PRIOR TO THE START OF CONSTRUCTION. ANY DISCREPANCIES SHALL BE REPORTED
- IMMEDIATELY TO THE ENGINEER.

 4. DESIGN ELEVATIONS GIVEN ARE TO BE ADHERED TO WITH NO CHANGES WITHOUT PRIOR WRITTEN APPROVAL BY ROBINSON LAND DEVELOPMENT.
- 5. ALL GROUND SURFACES SHALL BE EVENLY GRADED WITHOUT PONDING AREAS TO PROPOSED GRADES WHERE NOTED, AND EXISTING GRADES OTHERWISE.
- 6. CONTRACTOR SHALL ADJUST FINAL GRADE OF EXISTING MAINTENANCE HOLES, VALVE BOXES, ETC. AS REQUIRED TO MATCH PROPOSED GRADES.
 7. ANY AREAS BEYOND THE LIMIT OF THE SITE DISTURBED DURING CONSTRUCTION SHALL BE RESTORED TO ORIGINAL CONDITION OR BETTER TO THE SATISFACTION OF THE AUTHORITY HAVING JURISDICTION AT
- THE CONTRACTOR'S EXPENSE.

 8. RELOCATION OF EXISTING SERVICES AND/OR UTILITIES SHALL BE AS SHOWN ON THE DRAWINGS OR AS DIRECTED BY THE ENGINEER AT THE EXPENSE OF THE CONTRACTOR.
- 9. ALL WORK SHALL BE COMPLETED IN ACCORDANCE WITH THE "OCCUPATIONAL HEALTH AND SAFETY ACT AND REGULATIONS FOR CONSTRUCTION PROJECTS". THE GENERAL CONTRACTOR SHALL BE DEEMED TO
- AND REGULATIONS FOR CONSTRUCTION PROJECTS". THE GENERAL CONTRACTOR SHALL BE DEEMED TO BE THE CONSTRUCTOR AS DEFINED IN THE ACT.

 10. ALL CONSTRUCTION SIGNAGE MUST CONFORM TO THE M.T.O. MANUAL OF UNIFORM TRAFFIC CONTROL
- DEVICES (LATEST AMENDMENT).

 11. ALL DIMENSIONS ARE IN METERS UNLESS OTHERWISE SPECIFIED.
- 12. THE SUPPORT OF ALL UTILITIES SHALL BE IN ACCORDANCE WITH THE REQUIREMENTS OF THE AUTHORITY HAVING JURISDICTION.
 13. THE CONTRACTOR WILL BE RESPONSIBLE FOR ADDITIONAL BEDDING OR ADDITIONAL STRENGTH PIPE IF
- THE MAXIMUM TRENCH WIDTH, AS SPECIFIED BY OPSD, IS EXCEEDED.

 14. ALL NECESSARY CLEARING AND GRUBBING SHALL BE COMPLETED BY THE CONTRACTOR. REFER TO
- LANDSCAPE PLANS FOR ANY TREE CUTTING.

 15. REFER TO GEOTECHNICAL INVESTIGATION PREPARED BY KOLLAARD ASSOCIATES, DATED JUN 2025.

 16. THE CONTRACTOR IS RESPONSIBLE FOR AND SHALL PROVIDE FOR DEWATERING, SUPPORT AND
- PROTECTION OF EXCAVATIONS AND TRENCHING AS WELL AS RELEASE OF ANY PUMPED GROUNDWATER IN A CONTROLLED AND APPROVED MANNER.
- 17. DO NOT CONSTRUCT USING DRAWINGS THAT ARE NOT MARKED "ISSUED FOR CONSTRUCTION".
 18. CONTRACTOR IS RESPONSIBLE FOR ALL LAYOUT FOR CONSTRUCTION PURPOSES.
 19. THE CONTRACTOR SHALL BE RESPONSIBLE TO MANAGE EXCESS SOIL IN ACCORDANCE WITH ONTARIO REGULATION 406/19.

STORM SEWERS:

- 1. ALL REINFORCED CONCRETE STORM SEWER PIPE SHALL BE IN ACCORDANCE WITH CSA A257.2 (LATEST AMENDMENT). ALL NON-REINFORCED CONCRETE STORM SEWER PIPE SHALL BE IN ACCORDANCE WITH CSA A257.1 (LATEST AMENDMENT). PIPE SHALL BE JOINTED WITH STD. RUBBER GASKETS AS PER CSA A257.3
- (LAIES) AMENDMENT).

 2. ALL PVC STORM SEWERS ARE TO BE SDR 35 APPROVED PER C.S.A. B182.2 OR LATEST AMENDMENT,
 LINI ESS OTHERWISE SPECIFIED.
- UNLESS OTHERWISE SPECIFIED.

 3. ALL STORM SEWER TRENCH AND BEDDING SHALL BE IN ACCORDANCE WITH TOWN OF PERTH STD. SE-04 UNLESS OTHERWISE SPECIFIED. BEDDING AND COVER MATERIAL SHALL BE SPECIFIED BY GEOTECHNICAL
- 4. THE STORM SEWER CLASSES HAVE BEEN DESIGNED BASED ON BEDDING CONDITIONS SPECIFIED ABOVE. WHERE THE SPECIFIED TRENCH WIDTH IS EXCEEDED, THE CONTRACTOR SHALL BE REQUIRED TO PROVIDE ADDITIONAL BEDDING, A DIFFERENT TYPE OF BEDDING OR A HIGHER PIPE STRENGTH AT HIS OWN EXPENSE AND SHALL ALSO BE RESPONSIBLE FOR EXTRA TEMPORARY AND/OR PERMANENT REPAIRS MADE NECESSARY BY THE WIDENED TRENCH.
- ALL STORM MANHOLES SHALL BE 1200mm DIAMETER AS PER OPSD 701.010 UNLESS OTHERWISE NOTED.
 ALL CATCH BASINS SHALL BE 600mm X 600mm AS PER OPSD 705.010 UNLESS OTHERWISE NOTED.
 STORM MANHOLE FRAME AND COVERS SHALL BE AS PER OPSD 401.010
- 8. CB FRAME AND COVER PER OPSD 400.020
 9. STORM SEWER MANHOLES SERVING SEWERS LESS THAN 900mm SHALL BE CONSTRUCTED WITH A 300mm SUMP. FOR STORM SEWERS 900mm AND OVER USE BENCHING IN ACCORDANCE WITH OPSD 701.021.
 10. FOUNDATION DRAIN SUMP PUMP TO BE INSTALLED WITH BACKWATER VALVES (DESIGN BY OTHERS).

SANITARY SEWERS:

- 1. ALL SANITARY SEWERS SHALL BE PVC SDR 35 AND SERVICE LATERALS SHALL BE PVC SDR 28, IN
- ACCORDANCE WITH TOWN OF PERTH STANDARDS.

 2. SANITARY SEWER TRENCH AND BEDDING SHALL BE AS PER TOWN OF PERTH STD. SE-04 UNLESS OTHERWISE NOTED. BEDDING AND COVER MATERIAL SHALL BE SPECIFIED BY GEOTECHNICAL REPORT.

11. SEWERS WITH LESS THAN 1.4m COVER SHALL BE INSULATED PER TOWN OF PERTH STD. WA-02.

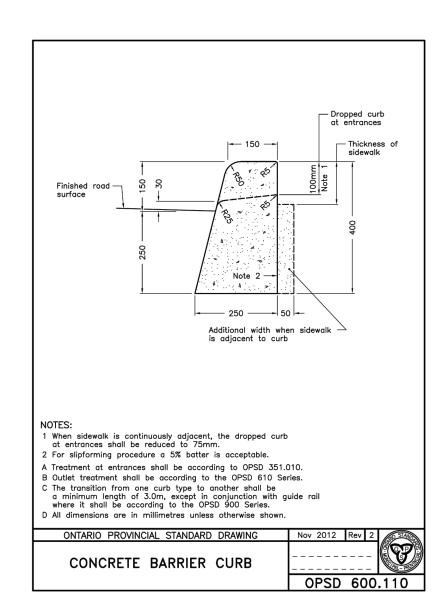
- 3. SUMP PUMP TO BE PROVIDED FOR BASEMENT FLOOR DRAIN (DESIGN BY OTHERS).
- WATER SUPPLY:
 1. ALL WATER SERVICES SHALL BE TYPE K SOFT COPPER CONFORMING TO ASTM B88.
- 2. WATERMAIN TRENCH AND BEDDING SHALL BE IN ACCORDANCE WITH TOWN OF PERTH STD. SE-04, UNLESS OTHERWISE SPECIFIED. BEDDING AND COVER MATERIAL SHALL BE SPECIFIED BY GEOTECHNICAL REPORT
- 3. CATHODIC PROTECTION IS REQUIRED ON ALL METALLIC FITTINGS AS PER TOWN OF PERTH REQUIREMENTS.
- CONCRETE CURB SHALL BE IN ACCORDANCE WITH OPSD 600.110. PROVISION SHALL BE MADE FOR CURB DEPRESSIONS AT SIDEWALKS AND DRIVEWAYS.
 ALL BARRIER CURB TO BE 150mm ABOVE FINISHED ASPHALT GRADE UNLESS OTHERWISE NOTED.
- CONCRETE SIDEWALK SHALL BE IN ACCORDANCE WITH OPSD 310.010 AND 310.020
 GRANULAR "A" SHALL BE PLACED TO A MINIMUM THICKNESS OF 300mm AROUND ALL STRUCTURES WITHIN
- PAVEMENT AREA.

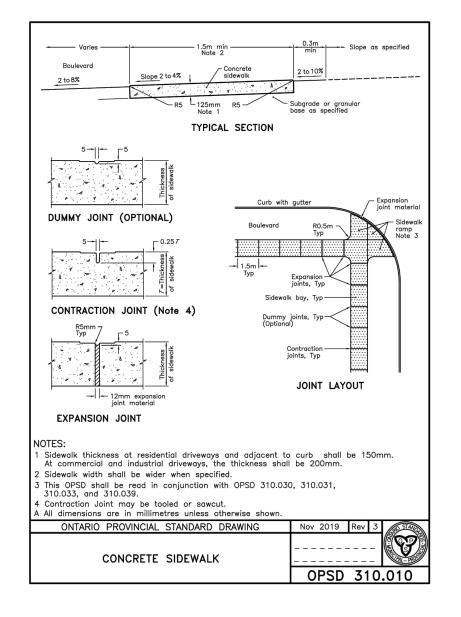
 5. ASPHALT WEAR COLLRSE SHALL NOT BE PLACED LINTH. THE VIDEO INSPECTION OF SEWERS & NECESSARY.
- 5. ASPHALT WEAR COURSE SHALL NOT BE PLACED UNTIL THE VIDEO INSPECTION OF SEWERS & NECESSARY REPAIRS HAVE BEEN CARRIED OUT TO THE SATISFACTION OF THE ENGINEER.

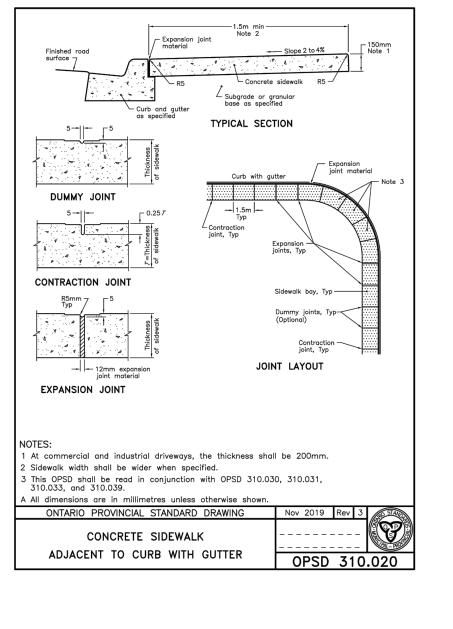
 6. SUB-EXCAVATE SOFT AREAS AND FILL WITH GRANULAR 'B' COMPACTED IN MAXIMUM 300mm LIFTS.
- 6. SUB-EXCAVATE SOFT AREAS AND FILL WITH GRANULAR B' COMPACTED IN MAXIMUM 300mm LIFTS.

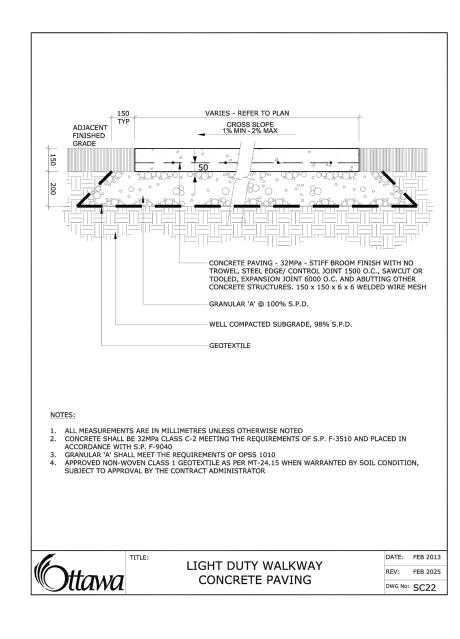
 7. ALL EDGES OF DISTURBED PAVEMENT SHALL BE SAW-CUT TO FORM A NEAT AND STRAIGHT LINE PRIOR TO
- 8. PAVEMENT DESIGN AS PER GEOTECHNICAL RECOMMENDATIONS. SEE REPORT BY KOLLAARD ASSOCIATES, DATED

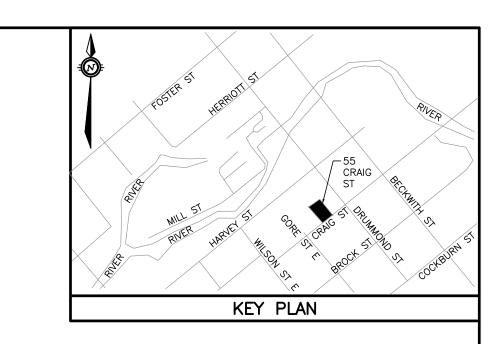
 JUN 2025

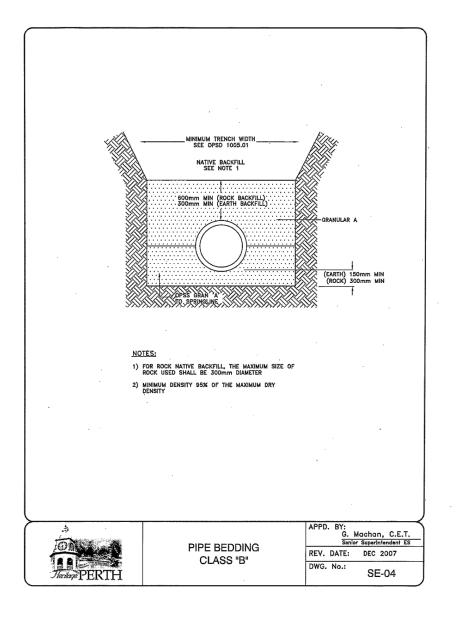


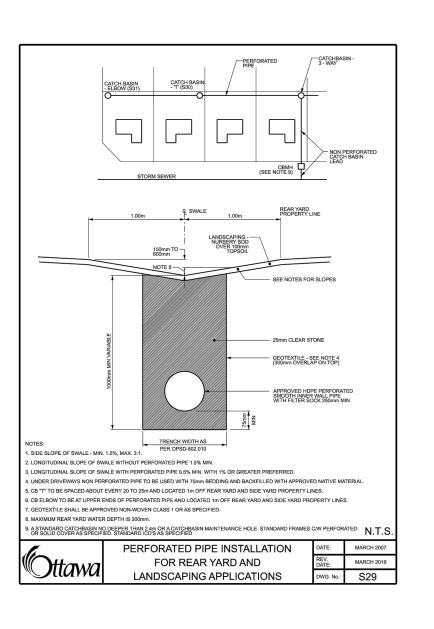


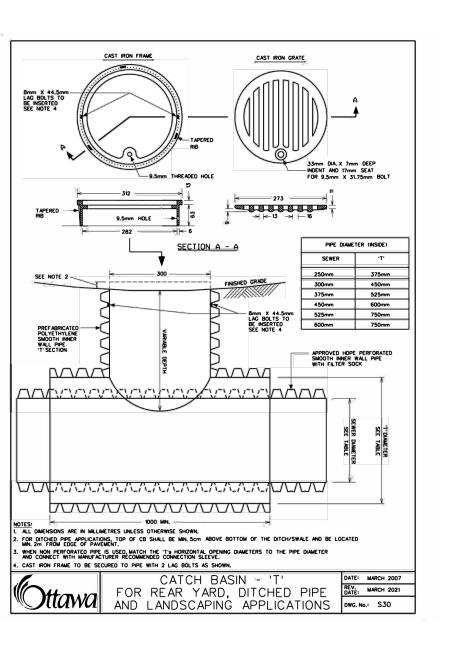


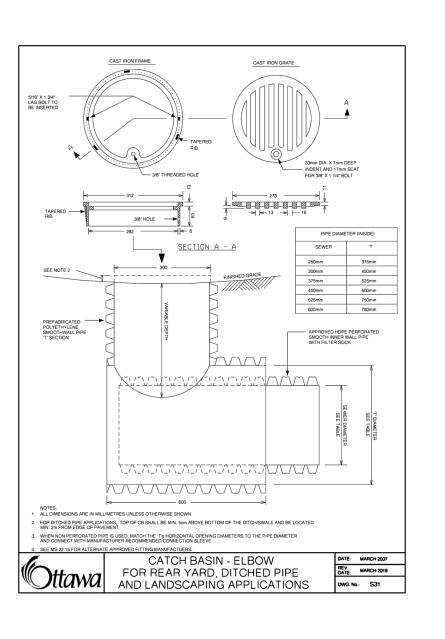












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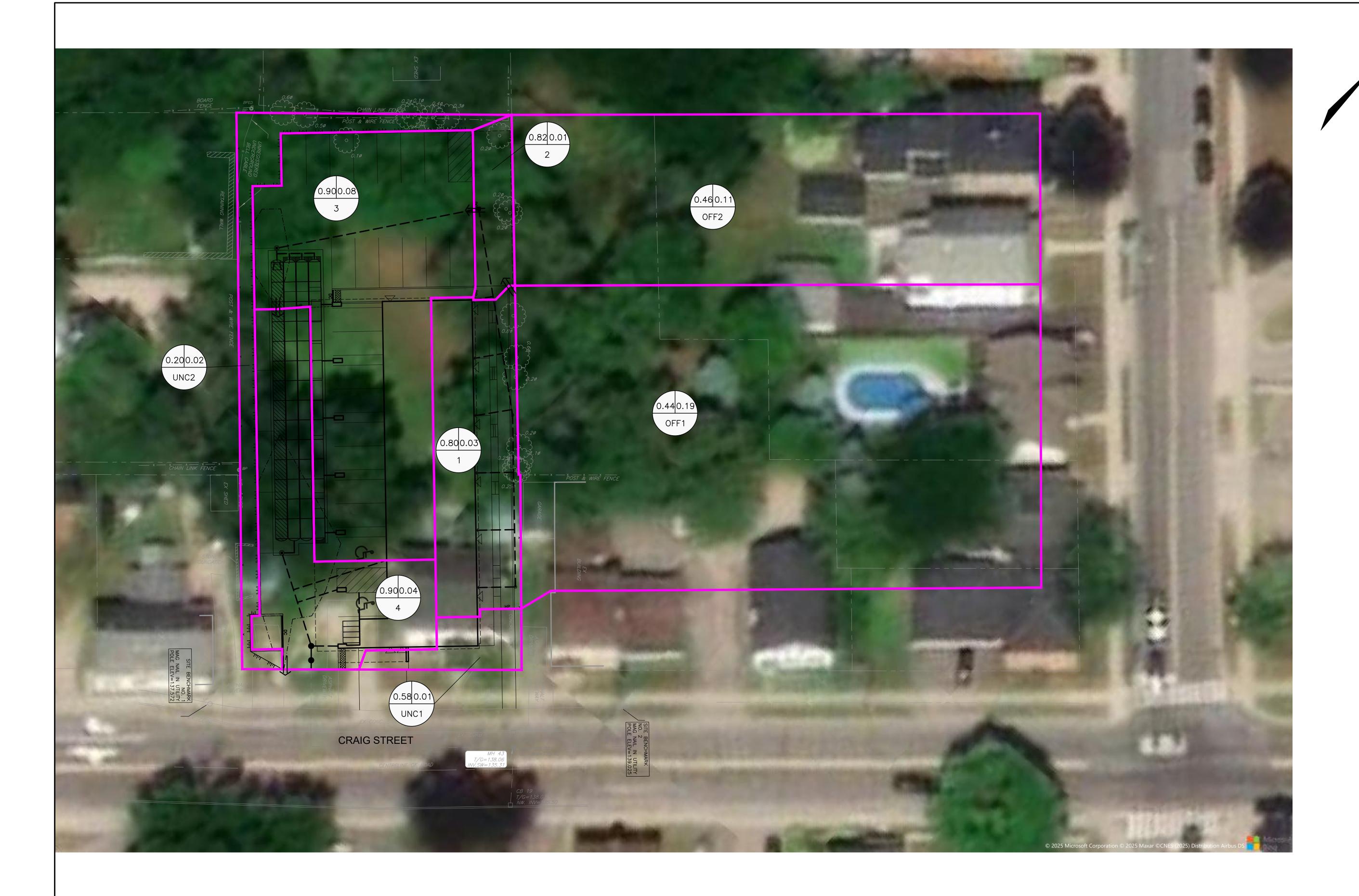
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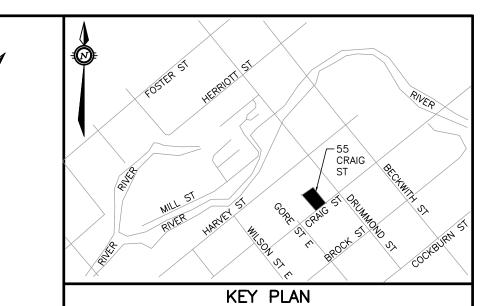
2B DEVELOPMENTS

55 CRAIG STREET, PERTH, ON NOTES AND DETAILS PLAN

PROJECT No.
24116
SURVEY
CD & AOV
DATED
JUNE 2025
DWG. No:

24110-N1





<u>LEGEND</u>

EXISTING CATCH BASIN

EXISTING STORM SEWER & MAINTENANCE HOLE

CATCH BASIN

REAR YARD CATCH BASIN

CATCH BASIN MAINTENANCE HOLE

STORM SEWER & MAINTENANCE HOLE

FITRANCE

TERRACING (3H:1V MAX.

STORM DRAINAGE AREA

O.50 0.28 AREA (ha)

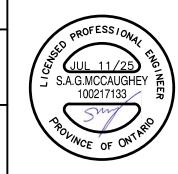
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DEVELOPMENTS

PERTH, ON

STORM DRAINAGE PLAN

PROJECT No.
24116
SURVEY
CD & AOV
DATED
JUNE 2025
DWG. No:
24116-STM1

Appendix C

Water Demand Calculations

Fire Demand Calculations

Hydrant Coverage Sketch



	R	ESIDENTIAL P	NON-RES			AVG. DAILY				MAX. DAILY				PEAK HOURLY								
Junction	ACTUAL COUNT					COMM.	INST.	INST. DEMAND (L/s)				DEMAND (L/s)				DEMAND (L/s)						
	Studio	1 Bedroom	2 Bedroom	Total	(ha)	(ha)	(ha)	RES.	IND.	COMM.	INST.	TOTAL	RES.	IND.	COMM.	INST.	TOTAL	RES.	IND.	COMM.	INST.	TOTAL
	Apartment	Apartment	Apartment	Population																		
																						1
BLDG		30		60				0.31				0.31	0.63				0.63	1.38				1.38
Total		30		60				0.31				0.31	0.63				0.63	1.38				1.38

Residential Densities
Low Density (SFH's) = 3.8 cap/unit Medium Density (Townhouses) = cap/unit

Apartments

Max. Daily Demand:

2.0 x Avg. Day

1.5 x Avg. Day

1.5 x Avg. Day Avg. Daily Demand:
Residential = 450 L/cap/day Peak Hourly Demand: 2.2 x Max. Day cap/unit cap/unit 1 Bedroom = 2.0 2 Bedroom = 3.0 Industrial (Light) = 35000 L/ha/day Commercial = 28000 L/ha/day Condo (Seniors) = cap/unit 1.8 x Max. Day 1.3 1.8 x Max. Day

> 2025-06-03 Page 1 of 1

Project Name: 53 Craig St.
Project Location: Perth, ON
Project No: 24116
Date: 12-May-25
Building Type: Residential
Building Being Considered: BLDG

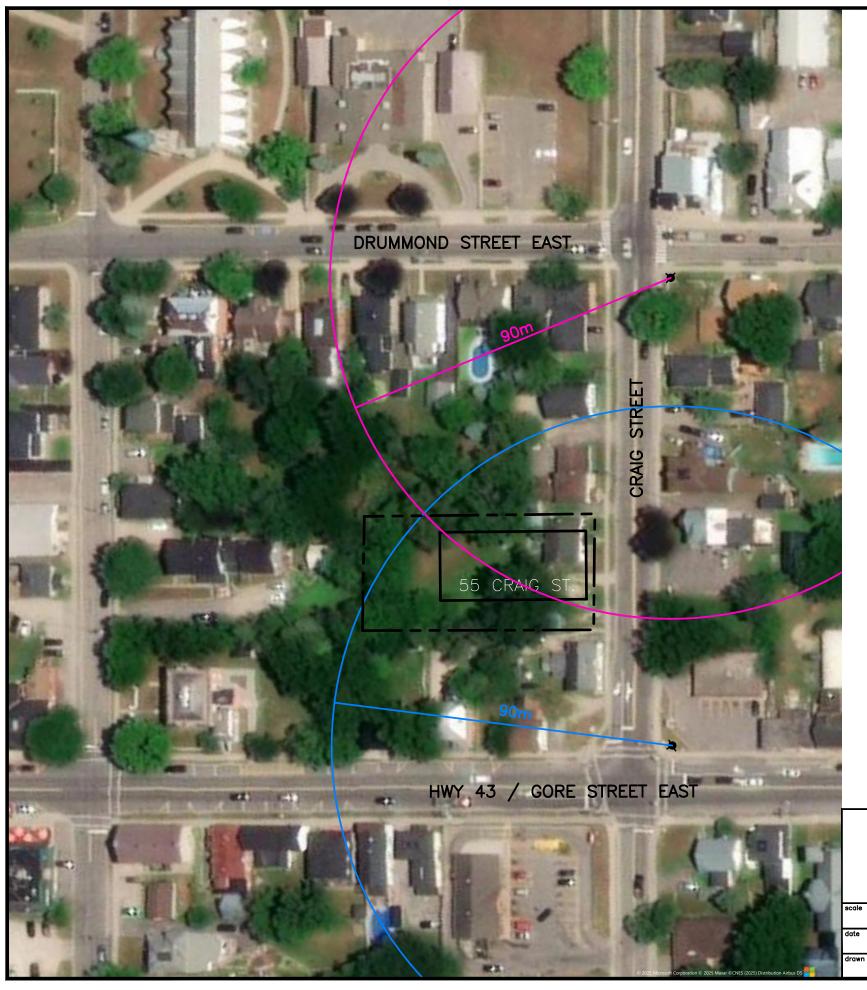
Exposures

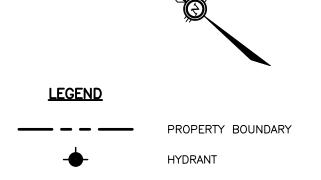
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Calculations for Total Required Fire Flow Value Step Parameter Options 1.5 Wood Frame (Type V) Type of Construction Ordinary Construction (Type III) 1.0 Wood Frame (Type V) Α 1.5 Non-Combustible Construction (Type II) 0.8 Fire Resistive Construction (Type I) Ground Floor Area 1711.0 В m² **Total Effective Floor Area** 1,711.0 С Fire Flow 14,000 L/min Options Charge Non-combustible -0.25 Limited Combustible -0.15 Limited Combustible **Occupancy Class** -0.15 Combustible 0.00 D Free burning 0.15 Rapid Burning 0.25 Occupancy Adjustment -2100 L/min Fire Flow 11,900 L/min Options Charge Automatic Sprinkler Protection -0.30 0.00 **Sprinkler Protection** None 0.00 Е Water Supply is Standard for System and Hose Lines -0.10 Nο 0.00 Full Supervision of the Sprinker System -0.10 No 0.00 Sprinkler Reduction L/min Exposures West Side (59 Craig St.) Subject Building and Exposed Building Fully Protected with Automatic Sprinker Systems No Exposed Building Fully Protected with Automatic Sprinker Systems No Exposed Wall Length 15 m Exposed Wall No. of Storeys 2 Length-Height Factor of Exposed Wall 30 m.storeys Options Ordinary with Unprotected Openings Construction Type of Exposed Wall Wood Frame Ordinary without Unprotected Openings Noncombustible or Fire Resistive with Unprotected Openings Noncombustible or Fire Resistive without Unprotected Openings Separation Distance m West Side (59 Craig St.) Exposure Charge 0.11

,soc sameg and Exposed building Ft	West Side (131 & 133 Gore St. E) Illy Protected with Automatic Sprinker Systems		No	
Exposed Building Fully Protected with Au			No	
Exposed Wall Length			18	
Exposed Wall No. of Storeys			2	
•			36	
Length-Height Factor of Exposed Wal			30	m.
	Options			
	Wood Frame			
Construction Type of Exposed Wall	Ordinary with Unprotected Openings	Wood Frame		
	Ordinary without Unprotected Openings			
	Noncombustible or Fire Resistive with Unprotected Openings			
	Noncombustible or Fire Resistive without Unprotected Openings			
Separation Distance			24	
West Side (131 & 133 Gore St. E) Expo			0.02	
	North Side			
Subject Building and Exposed Building Fu	Illy Protected with Automatic Sprinker Systems		No	
Exposed Building Fully Protected with Au	tomatic Sprinker Systems		No	
Exposed Wall Length			8	
Exposed Wall No. of Storeys			2	
Length-Height Factor of Exposed Wal	·		16	m.
	Options			_
	Wood Frame			
Construction Type of Evapped Wall	Ordinary with Unprotected Openings	Wood Frame		
Construction Type of Exposed Wall	Ordinary without Unprotected Openings	wood Frame		
	Noncombustible or Fire Resistive with Unprotected Openings			
	Noncombustible or Fire Resistive without Unprotected Openings			
Separation Distance		**>30m; No Exposure**	46	
North Side Exposure Charge			0.00	
	East Side			
Subject Building and Exposed Building Fu	Illy Protected with Automatic Sprinker Systems		No	
Exposed Building Fully Protected with Au			No	
Exposed Wall Length			20	
Exposed Wall No. of Storeys			2	
Length-Height Factor of Exposed Wal			40	m.
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	Wood Frame			
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Construction Type of Exposed Wall	Ordinary without Unprotected Openings	Wood Frame		
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Cti Di-t			8	
Separation Distance				
East Side Exposure Charge			0.16	
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East Side Exposure Charge Subject Building and Exposed Building Fu Exposed Building Fully Protected with Au Exposed Wall Length Exposed Wall No. of Storeys Length-Height Factor of Exposed Wal	South Side illy Protected with Automatic Sprinker Systems tomatic Sprinker Systems Coptions	Wood Frame	0.16 No No 9	m.:
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East Side Exposure Charge Subject Building and Exposed Building Fu Exposed Building Fully Protected with Au Exposed Wall Length Exposed Wall No. of Storeys Length-Height Factor of Exposed Wal	South Side ally Protected with Automatic Sprinker Systems tomatic Sprinker Systems Options Wood Frame Ordinary with Unprotected Openings Ordinary without Unprotected Openings	- Wood Frame	0.16 No No 9	m.
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East Side Exposure Charge Subject Building and Exposed Building Fu Exposed Building Fully Protected with Au Exposed Wall Length Exposed Wall No. of Storeys Length-Height Factor of Exposed Wall Construction Type of Exposed Wall	South Side Ally Protected with Automatic Sprinker Systems All Communities Sprinker Systems Options Wood Frame Ordinary with Unprotected Openings Ordinary without Unprotected Openings Noncombustible or Fire Resistive with Unprotected Openings Noncombustible or Fire Resistive without Unprotected Openings		0.16 No No 9 2 18	m.
East Side Exposure Charge Subject Building and Exposed Building Fu Exposed Building Fully Protected with Au Exposed Wall Length Exposed Wall No. of Storeys Length-Height Factor of Exposed Wall Construction Type of Exposed Wall	South Side Ally Protected with Automatic Sprinker Systems Atomatic Sprinker Systems Options Wood Frame Ordinary with Unprotected Openings Ordinary without Unprotected Openings Noncombustible or Fire Resistive with Unprotected Openings		0.16 No No 9 2 18	
East Side Exposure Charge Subject Building and Exposed Building Fu Exposed Building Fully Protected with Au Exposed Wall Length Exposed Wall No. of Storeys Length-Height Factor of Exposed Wall Construction Type of Exposed Wall Separation Distance South Side Exposure Charge	South Side ally Protected with Automatic Sprinker Systems from the Systems Options Wood Frame Ordinary with Unprotected Openings Ordinary without Unprotected Openings Noncombustible or Fire Resistive with Unprotected Openings		0.16 No No 9 2 18	m.
East Side Exposure Charge Subject Building and Exposed Building Fu Exposed Building Fully Protected with Au Exposed Wall Length Exposed Wall No. of Storeys Length-Height Factor of Exposed Wall Construction Type of Exposed Wall Separation Distance South Side Exposure Charge	South Side ally Protected with Automatic Sprinker Systems from the Systems Options Wood Frame Ordinary with Unprotected Openings Ordinary without Unprotected Openings Noncombustible or Fire Resistive with Unprotected Openings		0.16 No No 9 2 18 37 0.00	<

1. Fire flow calculations have been prepared in accordance with Fire Underwriters Survey (v. 2020)
2. Floor areas used in Step B based on all above-grade floors
3. Where buildings are at a diagonal to each other, the shortest separtion distance is increased by 3 metres and used as the exposure distance (Ref. FUS v.2020 pg.30).





NOT FOR CONSTRUCTION

Robinson

Land Development

	scale	CLIENT:	project no.
8	1:1000	2B Developments	24116
	date 70 /05 /05	ZD Developments	21110
	30/05/25	TITLE:	10.45
Ġ.	drawn by SM	Hydrant Coverage Sketch	HYD-1

Appendix D

Sanitary Sewer Design Sheet



LOCATION					UNIT COUNT		RESIDENTIAL AREA AND POPULATION				RESIDENTIAL FLOW			PIPE								
				S 550		INDIVIDUAL		CUMULATIVE				CUM. PEAK										
STREET	FROM MH		DRAINAGE AREA (ha)	STUDIO	1 BEDROOM	2 BEDROOM	POP.	AREA (ha)	POP.	AREA (ha)	PEAK FACTOR	PEAK POP. FLOW (L/s)	EXTRAN. FLOW (L/s)	DESIGN FLOW (L/s)	LENGTH (m)	DIAMETER (mm)	SLOPE (%)	CAPACITY (L/s)	FULL FLOW VELOCITY (m/s)	ACTUAL VELOCITY (m/s)	EXCESS CAPACITY (L/s)	PERCENT FULL
CRAIG ST.	BLDG	EX.SERVICE	0.19		30		60	0.19	60	0.19	4.00	0.97	0.05	1.02	1.5	150	2.0%	21.56	1.22	0.62	20.54	5%
CRAIG ST.	EX.SERVICE	EX.SAN	0.0						60	0.19	4.00	0.97	0.05	1.02	10	150	2.0%	21.56	1.22	0.62	20.54	5%

DESIGN PARAMETER	S
------------------	---

			Per Unit Populations:	
Average Daily Flow =	350	L/cap/day	Single Family	3.8 persons/unit
Commercial Flow =	28000	L/ha/day	Semi-detached	3.8 persons/unit
Industrial Flow =	35000	L/ha/day	Townhouse	3.5 persons/unit
Maximum Residential Peak Factor =	4.0		Apartments:	
Harmon - Correction Factor (K) =	1.00		1 Bedroom	2.0 persons/unit
Comm/Inst. Peak Factor =	1.5		2 Bedroom	3.0 persons/unit
Extraneous Flow =	0.28	L/s/ha	Condo (Seniors)	1.3 persons/unit
Minimum Full-Flow Velocity =	0.6	m/s		
Maximum Full-Flow Velocity =	2.4	m/s		

Page 1 of 1 2025-06-03

Appendix E

Pre- and Post-Development Flow Rates

Storm Sewer Design Sheets

ICD Calculations

Storage Volume Calculations

Underground Storage System Cutsheet

OGS Cutsheet



	Impervious	Pervious	Gravel
С	0.9	0.2	0.8

Runoff Coefficient Calculations - Pre-Development Runoff

Drainage Area ID	Impervious Area (ha)	Pervious Area (ha)	Gravel Area (ha)	Total Area (ha)	С	C (100 YR)	Percent Impervious (%)
PRE	0.001	0.001 0.180		0.186	0.22	0.28	3.5
	0.001	0.180	0.006	0.186	0.22	0.28	3.5

Runoff Coefficient Calculations - Site-Controlled Runoff

Drainage Area ID	Impervious Area (ha)	C		C (100 YR)	Percent Impervious (%)		
1	0.027	0.005	0.000	0.032	0.80	1.00	85.6
2	0.007	0.001	0.000	0.008	0.82	1.00	88.0
3	0.082	0.000	0.000	0.082	0.90	1.00	100.0
4	0.038	0.000	0.000	0.038	0.90	1.00	100.0
	0.154	0.006	0.000	0.160	0.88	1.00	96.5

Runoff Coefficient Calculations - Site-Uncontrolled Runoff

Drainage Area ID	Impervious Area (ha)	· C		С	C (100 YR)	Percent Impervious (%)	
UNC1	0.004	0.004	0.000	0.008	0.58	0.72	53.8
UNC2	0.000	0.019	0.000	0.019	0.20	0.25	0.0
-	0.004	0.022	0.000	0.027	0.31	0.39	16.2

Runoff Coefficient Calculations - Off-Site Runoff Entering Site

Drainage Area ID	Impervious Area (ha)	Pervious Area (ha)	Gravel Area (ha)	Total Area (ha)	С	C (100 YR)	Percent Impervious (%)
OFF1	0.066	0.127	0.000	0.193	0.44	0.55	34.2
OFF2	0.041	0.068	0.000	0.109	0.46	0.58	37.6
•	0.107	0 195	0.000	0.302	0.45	0.56	35.4

Note: $C_{100} = C * 1.25$ (max. 1.0)



Time of Concentration - Airport Method

Pre-Development Site incl. Off-Site (for Pre-Development Flows)

C = 0.36

L = 90 m

S = 2.5 %

Tc = 16.9

OFF1 & OFF2 Drainage Area (for Sewer Design Sheets)

C = 0.45

_ = 60 m

S = 2.0 %

Tc = 13.1

- 1. Tc = $3.26 \times (1.1 C) \times L^0.5 / S^0.33$
- 2. Slopes assumed based on "Craig Street Reconstruction" by Aplin Martin Consultants, IFC dated 06/10/2025



Pre-Development Flow Calculations (incl. Off-Site)

OFF1 & 2	Drainage Area	PRE	Drainage Area
0.302	Area (ha) =	0.186	Area (ha) =
0.45	C =	0.22	C =
0.56	C (100 YR) =	0.28	C (100 YR) =

Design Event	Time (min)	Rainfall Intensity (mm/hr)	On-Site Flow (L/s)	Off-Site Flow (L/s)	Total Flow (L/s)		
5 Year	16.9	77.9	8.9	29.3	38.2		
100 Year	16.9	133.2	19.1	62.6	81.7		

^{1.} Rainfall intensity calculated using Town of Perth IDF curve equations.

^{2.} Flow calculated using the Rational Method. Q=2.78CiA

^{3.} C (100 YR) = C + 25% (Max. 1.0)



Uncontrolled Flow Calculations

Area (ha) = 0.027

C = 0.31

C (100 YR) = 0.39

Design Event	Time (min)	Rainfall Intensity (mm/hr)	Flow (L/s)
5 Year	10	104.2	2.4
100 Year	10	178.6	5.2

- 1. Rainfall intensity calculated using Town of Perth IDF curve equations.
- 2. Flow calculated using the Rational Method. Q=2.78CiA
- 3. C (100 YR) = C + 25% (Max. 1.0)



	OCATION		AREA	/ha\			TIME OF	5 YR		CUMULATIVE					PROP	OSED SEWE	R			
L	LOCATION		AREA	(na)	INDIV.	ACCUM.	CONC			CONTROLLED	PIPE DIA	UPSTREAM	DNSTREAM	GRADE	LENGTH	CAPACITY	FULL FLOW	TIME OF	PERCENT	PERCENT
DRAINAGE AREA	FROM MH	то мн	TOTAL	l c	2.78AR	2.78AR	(min)		FLOW (L/s)	PEAK FLOW	(mm)	INV.	INV.	(%)	(m)	(L/s)	VELOCITY	FLOW	FULL	FULL
			AREA				, ,	(mm/hr)		(L/s)	, ,			(/	` '	(- /	(m/s)	(min)	(PEAK)	(CONTROLLED)
OFF1		RYCB	0.193	0.44	0.236	0.236	13.10	90.25	21.3	21.3										
1	RYCB	CB1	0.032	0.80	0.071	0.307	13.10	90.25	27.7	27.7	251	137.13	136.24	3.91	23.0	119.0	2.40	0.16	23%	23%
OFF2		CB1	0.109	0.46	0.140	0.140	13.10	90.25	12.7	12.7										
2	CB1	MH204	0.008	0.82	0.018	0.465	13.26	89.65	41.7	41.7	251	135.99	135.76	1.02	22.6	60.8	1.23	0.31	69%	69%
3	MH204	MH203	0.082	0.90	0.204	0.669	13.56	88.50	59.2	59.2		135.70	135.70	0.00	33.5					
4	MH203	MH202	0.038	0.90	0.095	0.764	13.56	88.50	67.7	67.7	299	135.67	135.57	0.93	10.7	92.5	1.32	0.14	73%	73%
	MH202	MH201	0.000	0.00	0.000	0.764	13.70	88.01	67.3	32.3	201	135.55	135.52	1.88	1.6	45.6	1.44	0.02	147%	71%
	MH201	EX. LAT	0.000	0.00	0.000	0.764	13.72	87.94	67.2	32.3	201	135.32	135.30	2.00	1.0	47.1	1.48	0.01	143%	69%
			0.462	0.60	0.764															
									Max	35.8										

Design Parameters

- Rainfall intensity calculated using Town of Perth IDF curve equations.
 Peak flows calculated using the Rational Method.
- 3. Manning's roughness coefficient = 0.013 4. Full flow velocity: MIN 0.8 m/s; MAX 6.0 m/s
- 6. MH204-MH203 is underground storage system (Stormtech SC-800 or equivalent). Refer to Servicing & Stormwater Management Report. 7. MH202 is controlled with ICD. Refer to ICD Sizing sheet.

- 8. Italicized "Cumulative Controlled Peak Flow" indicates the peak flow controlled by ICD.

 9. Max permitted flow discharging site = 5yr pre-development flow less uncontrolled flow plus off-site flow



	OCATION		ADEA	(ha)			TIME OF	100 YR	100 YR	CUMULATIVE					PROP	OSED SEWE	R			
L	OCATION		AREA	(na)	INDIV.	ACCUM.	CONC	RAINFALL	DEVK	CONTROLLED	PIPE DIA	UPSTREAM	DNSTREAM	GRADE	LENGTH	CAPACITY	FULL FLOW	TIME OF	PERCENT	PERCENT
DRAINAGE AREA	FROM MH	то мн	TOTAL AREA	С	2.78AR	2.78AR	(min)	INTENSITY (mm/hr)	FLOW (L/s)		(mm)	INV.	INV.	(%)	(m)	(L/s)	VELOCITY (m/s)	FLOW (min)	FULL (PEAK)	FULL (CONTROLLED)
			AILA					<u> </u>	Ī	(23)							(11113)	(111111)	(I EAR)	T(GOITTROELED)
OFF1		RYCB	0.193	0.55	0.295	0.295	13.10	154.46	45.5	45.5										
1	RYCB	CB1	0.032	1.00	0.089	0.384	13.10	154.46	59.2	59.2	251	137.13	136.24	3.91	23.0	119.0	2.40	0.16	50%	50%
OFF2		CB1	0.109	0.58	0.175	0.175	13.10	154.46	27.1	27.1										
2	CB1	MH204	0.008	1.00	0.022	0.581	13.26	153.41	89.2	89.2	251	135.99	135.76	1.02	22.6	60.8	1.23	0.31	147%	147%
3	MH204	MH203	0.082	1.00	0.227	0.808	13.56	151.43	122.3	122.3		135.70	135.70	0.00	33.5					
4	MH203	MH202	0.038	1.00	0.106	0.914	13.56	151.43	138.3	138.3	299	135.67	135.57	0.93	10.7	92.5	1.32	0.14	150%	150%
	MH202	MH201	0.000	0.00	0.000	0.914	13.70	150.58	137.6	32.3	201	135.55	135.52	1.88	1.6	45.6	1.44	0.02	302%	71%
	MH201	EX. LAT	0.000	0.00	0.000	0.914	13.72	150.47	137.5	32.3	201	135.32	135.30	2.00	1.0	47.1	1.48	0.01	292%	69%
			0.462	0.71	0.914															
									Max	76.6										

Design Parameters

- Rainfall intensity calculated using Town of Perth IDF curve equations.
 Peak flows calculated using the Rational Method.

- 3. Manning's roughness coefficient = 0.013 4. Full flow velocity: MIN 0.8 m/s; MAX 6.0 m/s
- 6. MH202 is controlled with ICD. Refer to ICD Sizing sheet.
- 7. Italicized "Cumulative Controlled Peak Flow" indicates the peak flow controlled by ICD.

 8. Max permitted flow discharging site = 100yr pre-development flow less uncontrolled flow plus off-site flow



ICD Sizing

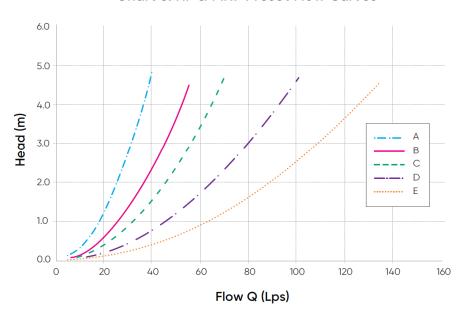
ST	NANA	H202
01	IVIIVI	11202

CL EI.	135.65	m
Top of U/G Storage	136.65	m
Head	1.00	m
Controlled Flow	32.3	L/s

HF C

1. Controlled flow based on head from centre of discharge pipe to top of underground storage (for sewer design sheet & storage)

Chart 3: HF & MHF Preset Flow Curves



Source: IPEX Tempest High Flow ICD

Flow & Storage Volume Calculations - Oversized Pipe

Accum. '2.78AR' - 5yr 0.764 Release Rate (L/s) = **32.3**

Accum. '2.78AR' - 100yr 0.914

Underground Storage System

Available Storage (m3) = 120.1

STMMH204

Oveflow EI. = 137.58 T/G = 137.49Ponding Area (m2) = 30.8

Available Storage (m3) = 3.7

STMMH203

Oveflow EI. = 137.44T/G = 137.31Ponding Area (m2) = 130.0

Available Storage (m3) = 8.5

Total Available Storage (m3) = 132.3

Design Event	Time (min)	Rainfall Intensity (mm/hr)	Flow (L/s)	Release Rate (L/s)	Net Runoff to be Stored (L/s)	Storage Required (m ³)
	10	76.8	58.7	16.2	42.5	25.5
	15	61.8	47.2	16.2	31.1	27.9
5 Year	20	52.0	39.8	16.2	23.6	28.3
5 Teal	25	45.2	34.5	16.2	18.4	27.5
	30	40.0	30.6	16.2	14.4	26.0
	35	36.1	27.6	16.2	11.4	23.9
	35	82.6	75.4	16.2	59.3	124.5
	40	75.1	68.6	16.2	52.5	126.0
100 Year	45	69.1	63.1	16.2	46.9	126.7
100 Tear	50	64.0	58.4	16.2	42.3	126.8
	55	59.6	54.5	16.2	38.3	126.4
	60	55.9	51.1	16.2	34.9	125.6

- 1. Rainfall intensity calculated using Town of Perth IDF curve equations.
- 3. Flow calculated using the Rational Method. Q=2.78CiA
- 4. C (100 YR) = C + 25% (Max. 1.0)
- $5. \ \ \text{Release Rate for storage calculation at 50\% max rate for average flow rate}. \ \ \text{See ICD Sizing sheet}$

PROJECT INFORMATION		
ENGINEERED PRODUCT MANAGER		
ADS SALES REP		
PROJECT NO.		





53 CRAIG ST PERTH, ON, CANADA

SC-800 STORMTECH CHAMBER SPECIFICATIONS

- CHAMBERS SHALL BE STORMTECH SC-800.
- 2. CHAMBERS SHALL BE ARCH-SHAPED AND SHALL BE MANUFACTURED FROM VIRGIN, IMPACT-MODIFIED POLYPROPYLENE COPOLYMERS
- CHAMBERS SHALL BE CERTIFIED TO CSA B184, "POLYMERIC SUB-SURFACE STORMWATER MANAGEMENT STRUCTURES", AND MEET THE REQUIREMENTS OF ASTM F2418, "STANDARD SPECIFICATION FOR POLYPROPYLENE (PP) CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- 4. CHAMBER ROWS SHALL PROVIDE CONTINUOUS, UNOBSTRUCTED INTERNAL SPACE WITH NO INTERNAL SUPPORTS THAT WOULD IMPEDE FLOW OR LIMIT ACCESS FOR INSPECTION.
- 5. THE STRUCTURAL DESIGN OF THE CHAMBERS, THE STRUCTURAL BACKFILL, AND THE INSTALLATION REQUIREMENTS SHALL ENSURE THAT THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS, SECTION 12.12, ARE MET FOR: 1) LONG-DURATION DEAD LOADS AND 2) SHORT-DURATION LIVE LOADS, BASED ON THE CSA S6 CL-625 TRUCK AND THE AASHTO DESIGN TRUCK WITH CONSIDERATION FOR IMPACT AND MULTIPLE VEHICLE PRESENCES.
- 6. CHAMBERS SHALL BE DESIGNED AND ALLOWABLE LOAD CONFIGURATIONS DETERMINED IN ACCORDANCE WITH ASTM F2787, "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS". LOAD CONFIGURATIONS SHALL INCLUDE: 1) INSTANTANEOUS (<1 MIN) AASHTO DESIGN TRUCK LIVE LOAD ON MINIMUM COVER 2) MAXIMUM PERMANENT (75-YR) COVER LOAD AND 3) ALLOWABLE COVER WITH PARKED (1-WEEK) AASHTO DESIGN TRUCK.
- 7. REQUIREMENTS FOR HANDLING AND INSTALLATION:
 - TO MAINTAIN THE WIDTH OF CHAMBERS DURING SHIPPING AND HANDLING, CHAMBERS SHALL HAVE INTEGRAL, INTERLOCKING STACKING LUGS.
 - TO ENSURE A SECURE JOINT DURING INSTALLATION AND BACKFILL, THE HEIGHT OF THE CHAMBER JOINT SHALL NOT BE LESS THAN 50 mm (2").
 - TO ENSURE THE INTEGRITY OF THE ARCH SHAPE DURING INSTALLATION, a) THE ARCH STIFFNESS CONSTANT SHALL BE GREATER THAN OR EQUAL TO 750 LBS/FT/%. THE ASC IS DEFINED IN SECTION 6.2.8 OF ASTM F2418. AND b) TO RESIST CHAMBER DEFORMATION DURING INSTALLATION AT ELEVATED TEMPERATURES (ABOVE 23° C / 73° F), CHAMBERS SHALL BE PRODUCED FROM REFLECTIVE GOLD OR YELLOW COLORS.
- 8. ONLY CHAMBERS THAT ARE APPROVED BY THE SITE DESIGN ENGINEER WILL BE ALLOWED. UPON REQUEST BY THE SITE DESIGN ENGINEER OR OWNER, THE CHAMBER MANUFACTURER SHALL SUBMIT A STRUCTURAL EVALUATION FOR APPROVAL BEFORE DELIVERING CHAMBERS TO THE PROJECT SITE AS FOLLOWS:
 - THE STRUCTURAL EVALUATION SHALL BE SEALED BY A REGISTERED PROFESSIONAL ENGINEER.
 - THE STRUCTURAL EVALUATION SHALL DEMONSTRATE THAT THE SAFETY FACTORS ARE GREATER THAN OR EQUAL TO 1.95 FOR DEAD LOAD AND 1.75 FOR LIVE LOAD, THE MINIMUM REQUIRED BY ASTM F2787 AND BY SECTIONS 3 AND 12.12 OF THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS FOR THERMOPLASTIC PIPE.
 - THE TEST DERIVED CREEP MODULUS AS SPECIFIED IN ASTM F2418 SHALL BE USED FOR PERMANENT DEAD LOAD DESIGN EXCEPT THAT IT SHALL BE THE 75-YEAR MODULUS USED FOR DESIGN.
- 9. CHAMBERS AND END CAPS SHALL BE PRODUCED AT AN ISO 9001 CERTIFIED MANUFACTURING FACILITY.
- 10. MANIFOLD SIZE TO BE DETERMINED BY SITE DESIGN ENGINEER. SEE TECH NOTE #6.32 FOR MANIFOLD SIZING GUIDANCE. DUE TO THE ADAPTATION OF THIS CHAMBER SYSTEM TO SPECIFIC SITE AND DESIGN CONSTRAINTS, IT MAY BE NECESSARY TO CUT AND COUPLE ADDITIONAL PIPE TO STANDARD MANIFOLD COMPONENTS IN THE FIELD.
- 11. ADS DOES NOT DESIGN OR PROVIDE MEMBRANE LINER SYSTEMS. TO MINIMIZE THE LEAKAGE POTENTIAL OF LINER SYSTEMS, THE MEMBRANE LINER SYSTEM SHOULD BE DESIGNED BY A KNOWLEDGEABLE GEOTEXTILE PROFESSIONAL AND INSTALLED BY A QUALIFIED CONTRACTOR.

IMPORTANT - NOTES FOR THE BIDDING AND INSTALLATION OF THE SC-800 SYSTEM

- 1. STORMTECH SC-800 CHAMBERS SHALL NOT BE INSTALLED UNTIL THE MANUFACTURER'S REPRESENTATIVE HAS COMPLETED A PRE-CONSTRUCTION MEETING WITH THE INSTALLERS.
- 2. STORMTECH SC-800 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH SC-310/SC-740/SC-800/DC-780 CONSTRUCTION GUIDE".
- 3. CHAMBERS ARE NOT TO BE BACKFILLED WITH A DOZER OR AN EXCAVATOR SITUATED OVER THE CHAMBERS. STORMTECH RECOMMENDS 3 BACKFILL METHODS:
 - STONESHOOTER LOCATED OFF THE CHAMBER BED.
 - BACKFILL AS ROWS ARE BUILT USING AN EXCAVATOR ON THE FOUNDATION STONE OR SUBGRADE.
 - BACKFILL FROM OUTSIDE THE EXCAVATION USING A LONG BOOM HOE OR EXCAVATOR.
- I. THE FOUNDATION STONE SHALL BE LEVELED AND COMPACTED PRIOR TO PLACING CHAMBERS.
- 5. JOINTS BETWEEN CHAMBERS SHALL BE PROPERLY SEATED PRIOR TO PLACING STONE.
- 6. MAINTAIN MINIMUM 75 mm (3") SPACING BETWEEN THE CHAMBER ROWS.
- 7. EMBEDMENT STONE SURROUNDING CHAMBERS MUST BE A CLEAN, CRUSHED, ANGULAR STONE OR RECYCLED CONCRETE; AASHTO M43 #3, 357, 4, 467, 5, 56, OR 57.
- 3. THE CONTRACTOR MUST REPORT ANY DISCREPANCIES WITH CHAMBER FOUNDATION MATERIALS BEARING CAPACITIES TO THE SITE DESIGN ENGINEER.
- . ADS RECOMMENDS THE USE OF "FLEXSTORM CATCH IT" INSERTS DURING CONSTRUCTION FOR ALL INLETS TO PROTECT THE SUBSURFACE STORMWATER MANAGEMENT SYSTEM FROM CONSTRUCTION SITE RUNOFF.

NOTES FOR CONSTRUCTION EQUIPMENT

- 1. STORMTECH SC-800 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH SC-310/SC-740/SC-800/DC-780 CONSTRUCTION GUIDE"
- THE USE OF CONSTRUCTION EQUIPMENT OVER SC-800 CHAMBERS IS LIMITED:
 - NO EQUIPMENT IS ALLOWED ON BARE CHAMBERS.
 - NO RUBBER TIRED LOADERS, DUMP TRUCKS, OR EXCAVATORS ARE ALLOWED UNTIL PROPER FILL DEPTHS ARE REACHED IN ACCORDANCE WITH THE "STORMTECH SC-310/SC-740/SC-800/DC-780 CONSTRUCTION GUIDE".
 - WEIGHT LIMITS FOR CONSTRUCTION EQUIPMENT CAN BE FOUND IN THE "STORMTECH SC-310/SC-740/SC-800/DC-780 CONSTRUCTION GUIDE".
- 3. FULL 900 mm (36") OF STABILIZED COVER MATERIALS OVER THE CHAMBERS IS REQUIRED FOR DUMP TRUCK TRAVEL OR DUMPING.

USE OF A DOZER TO PUSH EMBEDMENT STONE BETWEEN THE ROWS OF CHAMBERS MAY CAUSE DAMAGE TO THE CHAMBERS AND IS NOT AN ACCEPTABLE BACKFILL METHOD. ANY CHAMBERS DAMAGED BY THE "DUMP AND PUSH" METHOD ARE NOT COVERED UNDER THE STORMTECH STANDARD WARRANTY.

CONTACT STORMTECH AT 1-800-821-6710 WITH ANY QUESTIONS ON INSTALLATION REQUIREMENTS OR WEIGHT LIMITS FOR CONSTRUCTION EQUIPMENT.

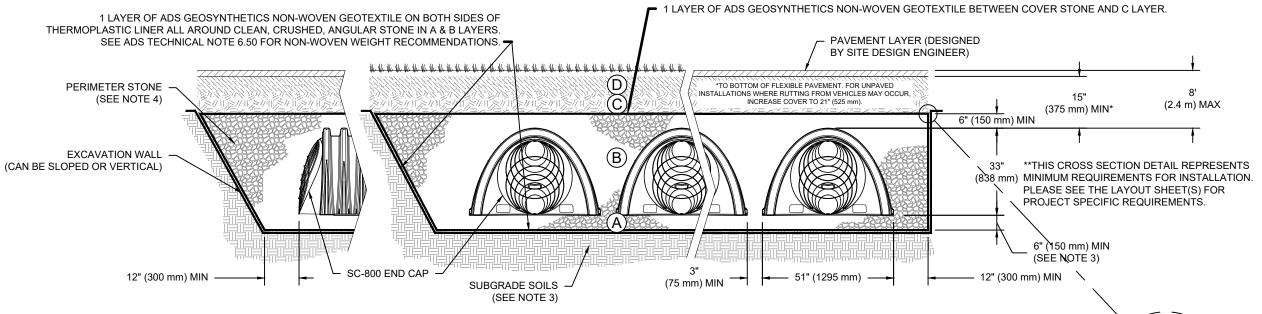
	SED LAYOUT	PROPOSED EL		PART TYPE	ITEM ON	*INVE DESCRIPTION	RT ABOVE BASE OF CHAMBER INVERT* MAX FLOW	
STORMTE	ECH SC-800 CHAMBERS ECH SC-800 END CAPS BOVE (mm)	MAXIMUM ALLOWABLE GRADE (TOP OF PAVE MINIMUM ALLOWABLE GRADE (UNPAVED WIT MINIMUM ALLOWABLE GRADE (UNPAVED NO	H TRAFFIC):	138.840 PART TYPE 136.935 136.783 PREFABRICATED EZ END CAP	LAYOUT	500 mm BOTTOM PREFABRICATED EZ END CAP, PART#: SC800ECEZ / TYP OF ALL 600 mm	58 mm	
	ELOW (mm)	MINIMUM ALLOWABLE GRADE (ONPAVED NO MINIMUM ALLOWABLE GRADE (TOP OF RIGID MINIMUM ALLOWABLE GRADE (BASE OF FLEX	CONCRÉTE PAVEMENT): 1	136.783 136.783 136.783 PRE-CORED END CAP		BOTTOM CONNECTIONS AND ISOLATOR PLUS ROWS 300 mm TOP PRE-CORED END CAP, PART#: SC800EPE12TPC / TYP OF ALL 300 mm TOP	366 mm	
INSTALLE	ED SYSTEM VOLUME (m³) LEVATION 135.614	TOP OF SC-800 CHAMBER:	, i	136.554 136.402 PRE-CORED END CAP		CONNECTIONS 300 mm BOTTOM PRE-CORED END CAP, PART#: SC800EPE12BPC / TYP OF ALL 300 mm BOTT	OM	AIG ST
(PERIMET	TER STONE INCLUDED) STONE INCLUDED)	300 mm x 300 mm TOP MANIFOLD INVERT: 300 mm x 300 mm TOP MANIFOLD INVERT:	1	135.929 135.929 FLAMP	C	CONNECTIONS NSTALL FLAMP ON 600 mm ACCESS PIPE / PART#: SC80024RAMP (TYP 2 PLACES)	41 mm	CRAIG TH, ON, CAN
SYSTEM A	AREA (m²) PERIMETER (m)	100 mm INSERTA TEE INVERT: 600 mm ISOLATOR ROW PLUS INVERT:	1	135.665 MANIFOLD 135.662 MANIFOLD	E	300 mm x 300 mm TOP MANIFOLD, ADS N-12 300 mm x 300 mm TOP MANIFOLD, ADS N-12	366 mm	ନ ବି
	PLASTIC LINER (m²)	600 mm ISOLATOR ROW PLUS INVERT: 300 mm BOTTOM CONNECTION INVERT:	1	135.622 PIPE CONNECTION 135.604 INSERTA TEE		300 mm BOTTOM CONNECTION 100 mm DIAMETER (TYP 5 PLACES)	41 mm 102 mm	~ ~
(2070 0 12		BOTTOM OF SC-800 CHAMBER: BOTTOM OF STONE:	1	135.563 CONCRETE STRUCTURE	i	(DESIGN BY ENGINEER / PROVIDED BY OTHERS)	130 L/s IN	4, [
		Serrom or Grone.		NYLOPLAST (OUTLET)	J K	(DESIGN BY ENGINEER / PROVIDED BY OTHERS) 750 mm DIAMETER (DESIGN BY ENGINEER)	167 L/s IN 57 L/s OUT	53
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	TOR ROW PLUS DETAIL)							8
 		SPLUS625 WOVEN GEOTEXTILE OVER EATH CHAMBER FEET FOR SCOUR INLET ROWS						7
BEDDI								
BEDDI PROTE THERN	MOPLASTIC LINER (SEE TI GN BY OTHERS)	ECH NOTE #6.50 PROVIDED BY OTHERS /	NOTES					SHE

ACCEPTABLE FILL MATERIALS: STORMTECH SC-800 CHAMBER SYSTEMS

	MATERIAL LOCATION	DESCRIPTION	AASHTO MATERIAL CLASSIFICATIONS	COMPACTION / DENSITY REQUIREMENT
D	FINAL FILL: FILL MATERIAL FOR LAYER 'D' STARTS FROM THE TOP OF THE 'C' LAYER TO THE BOTTOM OF FLEXIBLE PAVEMENT OR UNPAVED FINISHED GRADE ABOVE. NOTE THAT PAVEMENT SUBBASE MAY BE PART OF THE 'D' LAYER.	ANY SOIL/ROCK MATERIALS, NATIVE SOILS, OR PER ENGINEER'S PLANS. CHECK PLANS FOR PAVEMENT SUBGRADE REQUIREMENTS.	N/A	PREPARE PER SITE DESIGN ENGINEER'S PLANS. PAVED INSTALLATIONS MAY HAVE STRINGENT MATERIAL AND PREPARATION REQUIREMENTS.
С	INITIAL FILL: FILL MATERIAL FOR LAYER 'C' STARTS FROM THE TOP OF THE EMBEDMENT STONE ('B' LAYER) TO 15" (375 mm) ABOVE THE TOP OF THE CHAMBER. NOTE THAT PAVEMENT SUBBASE MAY BE A PART OF THE 'C' LAYER.	GRANULAR WELL-GRADED SOIL/AGGREGATE MIXTURES, <35% FINES OR PROCESSED AGGREGATE. MOST PAVEMENT SUBBASE MATERIALS CAN BE USED IN LIEU OF THIS LAYER.	AASHTO M145 ¹ A-1, A-2-4, A-3 OR AASHTO M43 ¹ 3, 357, 4, 467, 5, 56, 57, 6, 67, 68, 7, 78, 8, 89, 9, 10	BEGIN COMPACTIONS AFTER 12" (300 mm) OF MATERIAL OVER THE CHAMBERS IS REACHED. COMPACT ADDITIONAL LAYERS IN 6" (150 mm) MAX LIFTS TO A MIN. 95% PROCTOR DENSITY FOR WELL GRADED MATERIAL AND 95% RELATIVE DENSITY FOR PROCESSED AGGREGATE MATERIALS. ROLLER GROSS VEHICLE WEIGHT NOT TO EXCEED 12,000 lbs (53 kN). DYNAMIC FORCE NOT TO EXCEED 20,000 lbs (89 kN).
В	EMBEDMENT STONE: FILL SURROUNDING THE CHAMBERS FROM THE FOUNDATION STONE ('A' LAYER) TO THE 'C' LAYER ABOVE.	CLEAN, CRUSHED, ANGULAR STONE OR RECYCLED CONCRETE ⁵	AASHTO M43 ¹ 3, 357, 4, 467, 5, 56, 57	NO COMPACTION REQUIRED.
А	FOUNDATION STONE: FILL BELOW CHAMBERS FROM THE SUBGRADE UP TO THE FOOT (BOTTOM) OF THE CHAMBER.	CLEAN, CRUSHED, ANGULAR STONE OR RECYCLED CONCRETE ⁵	AASHTO M43¹ 3, 357, 4, 467, 5, 56, 57	PLATE COMPACT OR ROLL TO ACHIEVE A FLAT SURFACE. ^{2,3}

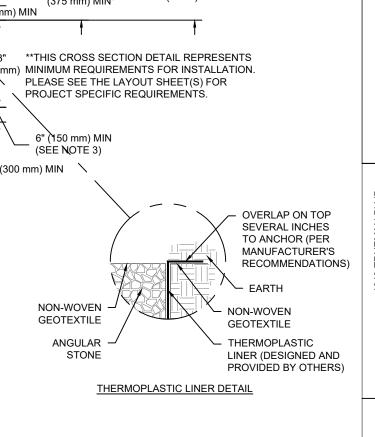
PLEASE NOTE:

- 1. THE LISTED AASHTO DESIGNATIONS ARE FOR GRADATIONS ONLY. THE STONE MUST ALSO BE CLEAN, CRUSHED, ANGULAR. FOR EXAMPLE, A SPECIFICATION FOR #4 STONE WOULD STATE: "CLEAN, CRUSHED, ANGULAR NO. 4 (AASHTO M43) STONE".
- 2. STORMTECH COMPACTION REQUIREMENTS ARE MET FOR 'A' LOCATION MATERIALS WHEN PLACED AND COMPACTED IN 6" (150 mm) (MAX) LIFTS USING TWO FULL COVERAGES WITH A VIBRATORY COMPACTOR.
- 3. WHERE INFILTRATION SURFACES MAY BE COMPROMISED BY COMPACTION, FOR STANDARD DESIGN LOAD CONDITIONS, A FLAT SURFACE MAY BE ACHIEVED BY RAKING OR DRAGGING WITHOUT COMPACTION EQUIPMENT. FOR SPECIAL LOAD DESIGNS, CONTACT STORMTECH FOR COMPACTION REQUIREMENTS
- 4. ONCE LAYER 'C' IS PLACED, ANY SOIL/MATERIAL CAN BE PLACED IN LAYER 'D' UP TO THE FINISHED GRADE. MOST PAVEMENT SUBBASE SOILS CAN BE USED TO REPLACE THE MATERIAL REQUIREMENTS OF LAYER 'C' OR 'D' AT THE SITE DESIGN ENGINEER'S DISCRETION.
- 5. WHERE RECYCLED CONCRETE AGGREGATE IS USED IN LAYERS 'A' OR 'B' THE MATERIAL SHOULD ALSO MEET THE ACCEPTABILITY CRITERIA OUTLINED IN TECHNICAL NOTE 6.20 "RECYCLED CONCRETE STRUCTURAL BACKFILL".



NOTES:

- 1. CHAMBERS SHALL MEET THE REQUIREMENTS OF ASTM F2418, "STANDARD SPECIFICATION FOR POLYPROPYLENE (PP) CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- 2. SC-800 CHAMBERS SHALL BE DESIGNED IN ACCORDANCE WITH ASTM F2787 "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- 3. THE SITE DESIGN ENGINEER IS RESPONSIBLE FOR ASSESSING THE BEARING RESISTANCE (ALLOWABLE BEARING CAPACITY) OF THE SUBGRADE SOILS AND THE DEPTH OF FOUNDATION STONE WITH CONSIDERATION FOR THE RANGE OF EXPECTED SOIL MOISTURE CONDITIONS. REFERENCE STORMTECH DESIGN MANUAL FOR BEARING CAPACITY GUIDANCE.
- 4. PERIMETER STONE MUST BE EXTENDED HORIZONTALLY TO THE EXCAVATION WALL FOR BOTH VERTICAL AND SLOPED EXCAVATION WALLS.
- 5. REQUIREMENTS FOR HANDLING AND INSTALLATION:
 - TO MAINTAIN THE WIDTH OF CHAMBERS DURING SHIPPING AND HANDLING, CHAMBERS SHALL HAVE INTEGRAL, INTERLOCKING STACKING LUGS.
 - TO ENSURE A SECURE JOINT DURING INSTALLATION AND BACKFILL, THE HEIGHT OF THE CHAMBER JOINT SHALL NOT BE LESS THAN 2".
 - TO ENSURE THE INTEGRITY OF THE ARCH SHAPE DURING INSTALLATION, a) THE ARCH STIFFNESS CONSTANT AS DEFINED IN SECTION 6.2.8 OF ASTM F2418 SHALL BE GREATER THAN OR EQUAL TO 750 LBS/FT/%. AND b) TO RESIST CHAMBER DEFORMATION DURING INSTALLATION AT ELEVATED TEMPERATURES (ABOVE 73° F / 23° C), CHAMBERS SHALL BE PRODUCED FROM REFLECTIVE GOLD OR YELLOW COLORS.



PERTH, ON, CANADA 2025 DRAWN: HN CHECKED: N

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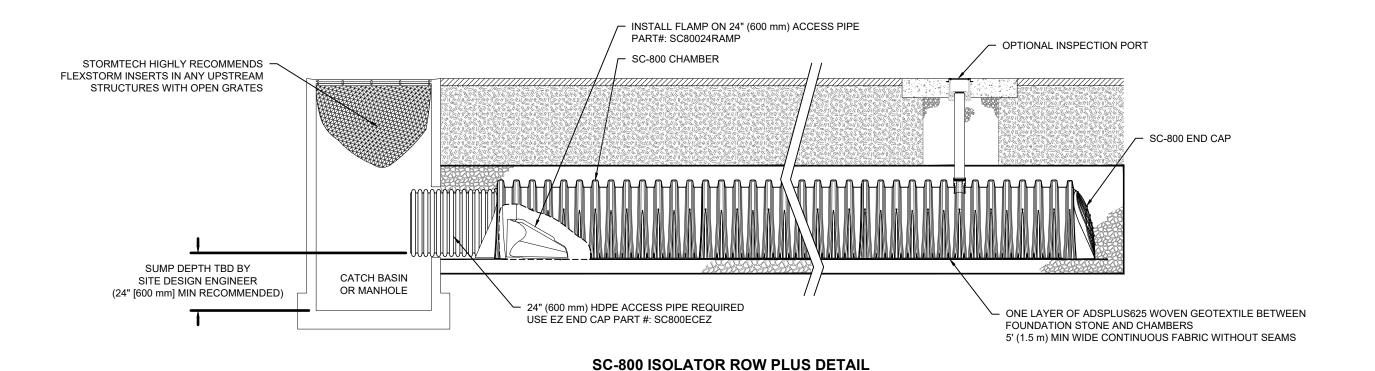
53

StormTech®

Chamber System

SHEET

3 OF 6



INSPECTION & MAINTENANCE

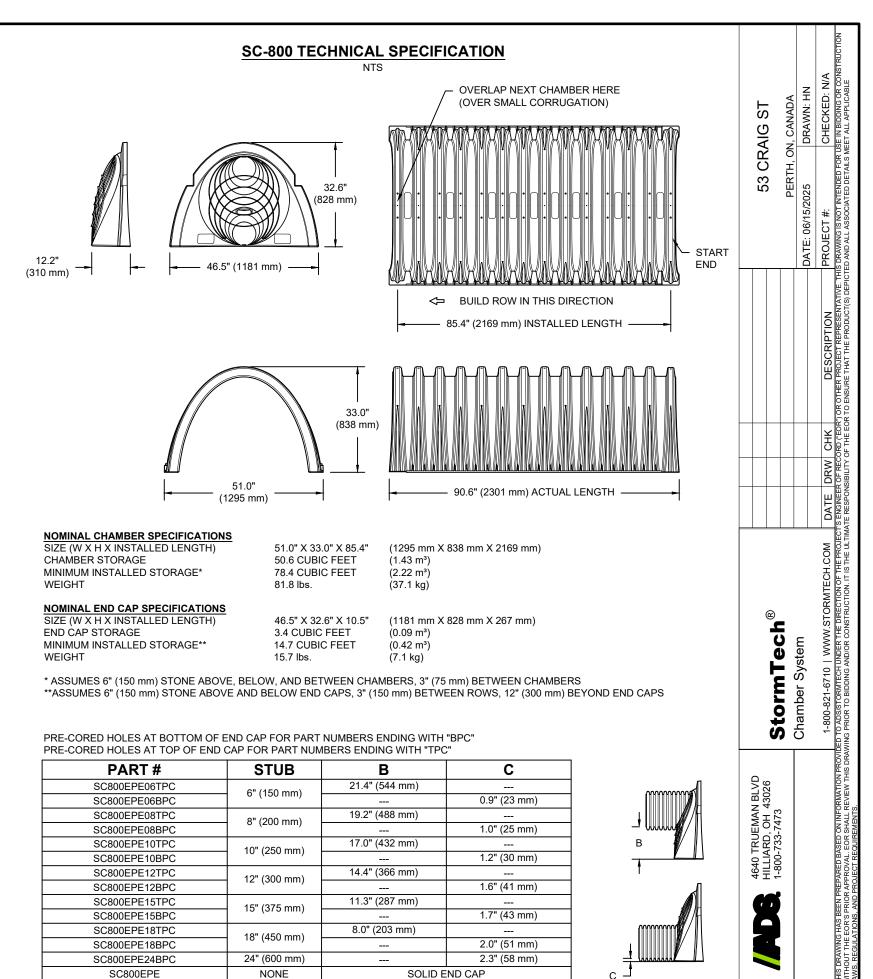
INSPECT ISOLATOR ROW PLUS FOR SEDIMENT

- A. INSPECTION PORTS (IF PRESENT)
- REMOVE/OPEN LID ON NYLOPLAST INLINE DRAIN
- REMOVE AND CLEAN FLEXSTORM FILTER IF INSTALLED
- USING A FLASHLIGHT AND STADIA ROD, MEASURE DEPTH OF SEDIMENT AND RECORD ON MAINTENANCE LOG LOWER A CAMERA INTO ISOLATOR ROW PLUS FOR VISUAL INSPECTION OF SEDIMENT LEVELS (OPTIONAL)
- IF SEDIMENT IS AT, OR ABOVE, 3" (80 mm) PROCEED TO STEP 2. IF NOT, PROCEED TO STEP 3.
- B. ALL ISOLATOR PLUS ROWS
- REMOVE COVER FROM STRUCTURE AT UPSTREAM END OF ISOLATOR ROW PLUS
- USING A FLASHLIGHT, INSPECT DOWN THE ISOLATOR ROW PLUS THROUGH OUTLET PIPE
 - i) MIRRORS ON POLES OR CAMERAS MAY BE USED TO AVOID A CONFINED SPACE ENTRY
 - ii) FOLLOW OSHA REGULATIONS FOR CONFINED SPACE ENTRY IF ENTERING MANHOLE
- IF SEDIMENT IS AT, OR ABOVE, 3" (80 mm) PROCEED TO STEP 2. IF NOT, PROCEED TO STEP 3.
- CLEAN OUT ISOLATOR ROW PLUS USING THE JETVAC PROCESS
 - A. A FIXED CULVERT CLEANING NOZZLE WITH REAR FACING SPREAD OF 45" (1.1 m) OR MORE IS PREFERRED
 - APPLY MULTIPLE PASSES OF JETVAC UNTIL BACKFLUSH WATER IS CLEAN
 - C. VACUUM STRUCTURE SUMP AS REQUIRED
- REPLACE ALL COVERS, GRATES, FILTERS, AND LIDS; RECORD OBSERVATIONS AND ACTIONS.
- INSPECT AND CLEAN BASINS AND MANHOLES UPSTREAM OF THE STORMTECH SYSTEM. STEP 4)

NOTES

- INSPECT EVERY 6 MONTHS DURING THE FIRST YEAR OF OPERATION. ADJUST THE INSPECTION INTERVAL BASED ON PREVIOUS OBSERVATIONS OF SEDIMENT ACCUMULATION AND HIGH WATER ELEVATIONS.
- 2. CONDUCT JETTING AND VACTORING ANNUALLY OR WHEN INSPECTION SHOWS THAT MAINTENANCE IS NECESSARY.

PERTH, ON, CANADA 2025 DRAWN: HN CHECKED: N ST CRAIG 53 **StormTech**[®] Chamber System 4640 TRUEMAN BLVD HILLIARD, OH 43026 1-800-733-7473 SHEET 4 OF 6

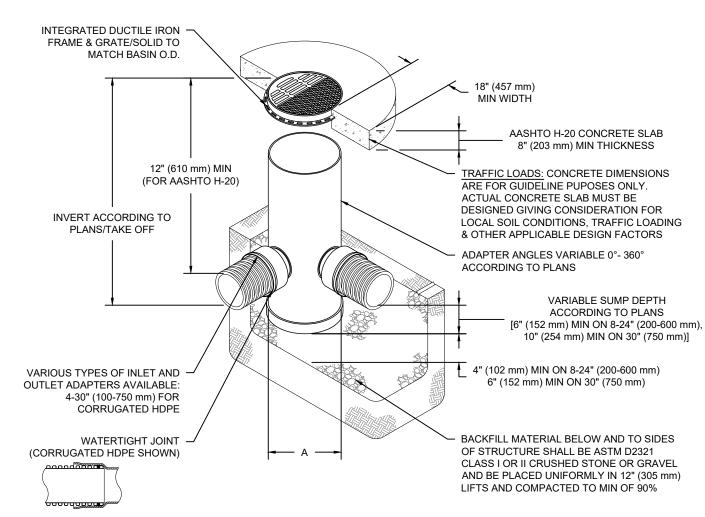


NOTE: ALL DIMENSIONS ARE NOMINAL

SHEET

5 OF 6

NYLOPLAST DRAIN BASIN

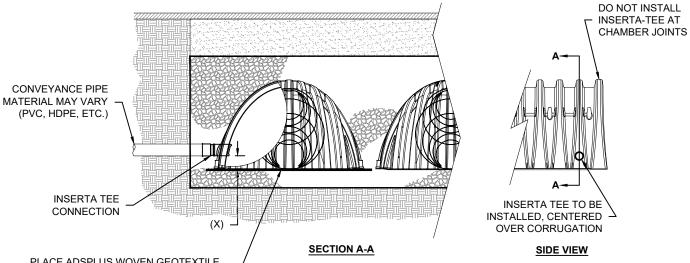


NOTES

- 8-30" (200-750 mm) GRATES/SOLID COVERS SHALL BE DUCTILE IRON PER ASTM A536 GRADE 70-50-05
- 12-30" (300-750 mm) FRAMES SHALL BE DUCTILE IRON PER ASTM A536 GRADE 70-50-05 DRAIN BASIN TO BE CUSTOM MANUFACTURED ACCORDING TO PLAN DETAILS
- DRAINAGE CONNECTION STUB JOINT TIGHTNESS SHALL CONFORM TO ASTM D3212 FOR CORRUGATED HDPE (ADS & HANCOR DUAL WALL) & SDR 35 PVC
- FOR COMPLETE DESIGN AND PRODUCT INFORMATION: WWW.NYLOPLAST-US.COM
- TO ORDER CALL: 800-821-6710

Α	PART#	GRATE/SOLID COVER OPTIONS		
8" (200 mm)	2808AG	PEDESTRIAN LIGHT DUTY	STANDARD LIGHT DUTY	SOLID LIGHT DUTY
10" (250 mm)	2810AG	PEDESTRIAN LIGHT DUTY	STANDARD LIGHT DUTY	SOLID LIGHT DUTY
12"	2812AG	PEDESTRIAN	STANDARD AASHTO	SOLID
(300 mm)		AASHTO H-10	H-20	AASHTO H-20
15"	2815AG	PEDESTRIAN	STANDARD AASHTO	SOLID
(375 mm)		AASHTO H-10	H-20	AASHTO H-20
18"	2818AG	PEDESTRIAN	STANDARD AASHTO	SOLID
(450 mm)		AASHTO H-10	H-20	AASHTO H-20
24"	2824AG	PEDESTRIAN	STANDARD AASHTO	SOLID
(600 mm)		AASHTO H-10	H-20	AASHTO H-20
30"	2830AG	PEDESTRIAN	STANDARD AASHTO	SOLID
(750 mm)		AASHTO H-20	H-20	AASHTO H-20

INSERTA TEE DETAIL



CHAMBER

SC-310

SC-800

DC-780

MC-3500

MC-4500

PLACE ADSPLUS WOVEN GEOTEXTILE (CENTERED ON INSERTA-TEE INLET) OVER BEDDING STONE FOR SCOUR PROTECTION AT SIDE INLET CONNECTIONS. GEOTEXTILE MUST EXTEND 6" (150 mm) PAST CHAMBER FOOT

NOTES:

- PART NUMBERS WILL VARY BASED ON INLET PIPE MATERIALS. CONTACT STORMTECH FOR MORE INFORMATION
- CONTACT ADS ENGINEERING SERVICES IF INSERTA TEE INLET MUST BE RAISED AS NOT ALL INVERTS ARE POSSIBLE.

MAX DIAMETER OF INSERTA TEE	HEIGHT FROM BASE OF CHAMBER (X)
6" (150 mm)	4" (100 mm)
10" (250 mm)	4" (100 mm)

4" (100 mm)

6" (150 mm)

8" (200 mm)

MC-7200 12" (300 mm) 8" (200 mm) INSERTA TEE FITTINGS AVAILABLE FOR SDR 26, SDR 35, SCH 40 IPS GASKETED & SOLVENT WELD, N-12, HP STORM, C-900 OR DUCTILE IRON

10" (250 mm)

12" (300 mm)

12" (300 mm)

Nyloplast®

PERTH, ON, CANADA 1025 DRAWN: HN CHECKED: N/

06/15/2025

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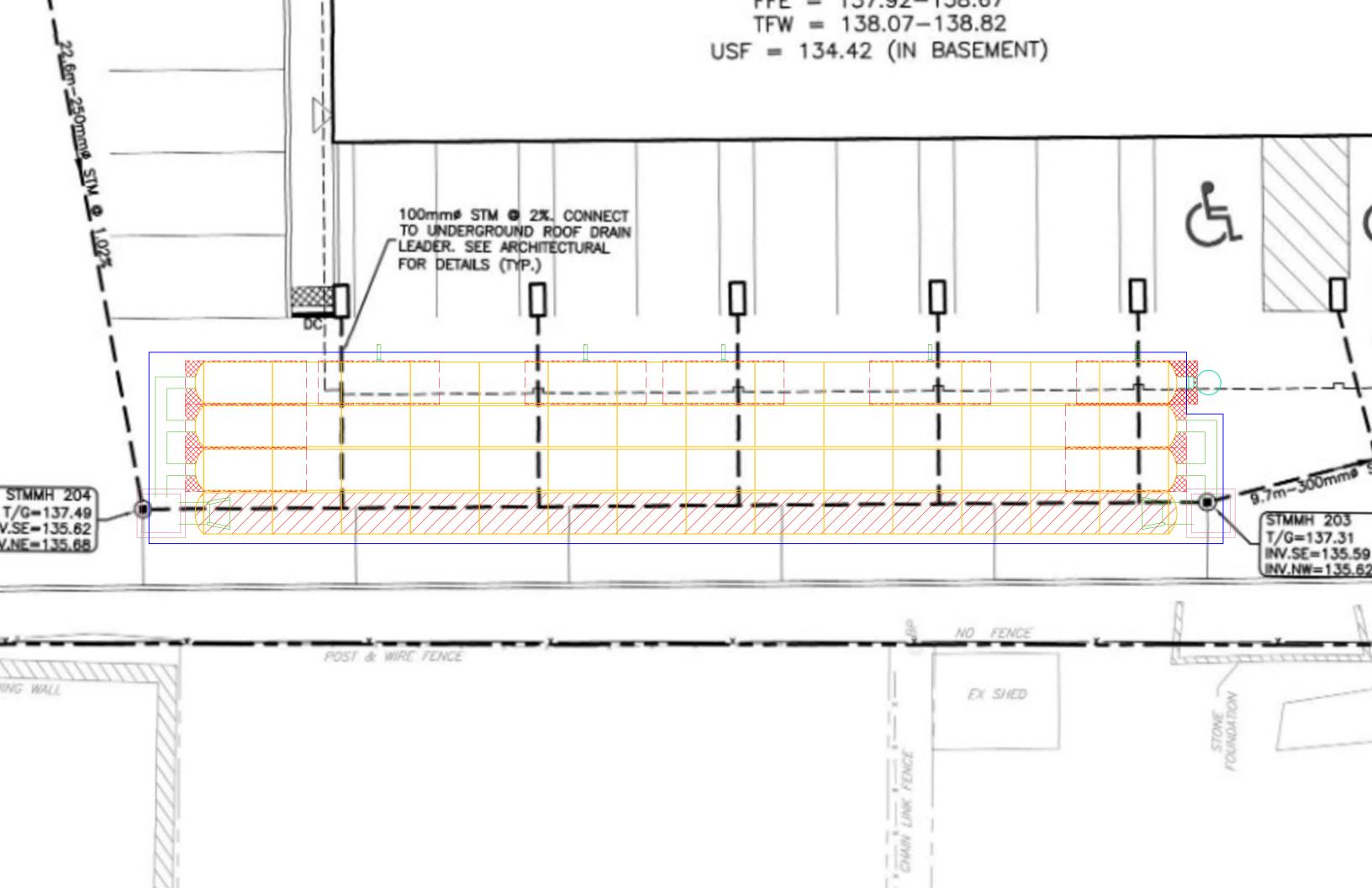
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4640 TRUEMAN BLVD HILLIARD, OH 43026 1-800-733-7473



SHEET

6 OF 6







ADS OGS Sizing Summary

Project Name: 53 Craig St

Consulting Engineer: Robinson Consultants Inc

Location: Perth, Ontario

Sizing Completed By: Haider Nasrullah Email: haider.nasrullah@adspipe.com

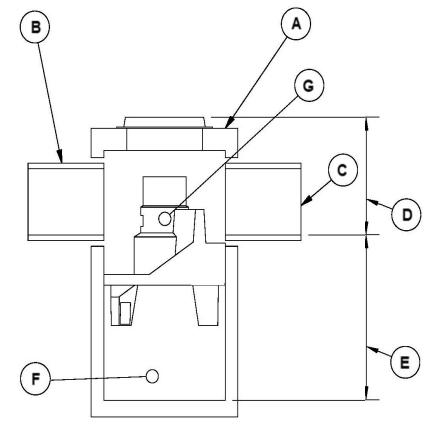
Treatment Requirements				
Treatment Goal:	Enhanced (MOE)			
Selected Parameters:	80% TSS 90% Volume			
Selected Unit:	FD-4HC			

Summary of Results				
Model	TSS Removal	Volume Treated		
FD-4HC	94.0%	>90%		
FD-5HC	96.0%	>90%		
FD-6HC	97.0%	>90%		
FD-8HC	98.0%	>90%		
FD-10HC	99.0%	>90%		

FD-4HC Specification				
Unit Diameter (A):	1,200 mm			
Inlet Pipe Diameter (B):	200 mm			
Outlet Pipe Diameter (C):	200 mm			
Height, T/G to Outlet Invert (D):	2470 mm			
Height, Outlet Invert to Sump (E):	1515 mm			
Sediment Storage Capacity (F):	0.78 m³			
Oil Storage Capacity (G):	723 L			
Recommended Sediment Depth for Maintenance:	440 mm			
Max. Pipe Diameter:	600 mm			
Peak Flow Capacity:	510 L/s			

Site Elevations:		
Rim Elevation:	137.59	
Inlet Pipe Elevation:	135.42,	
Outlet Pipe Elevation:	135.12	

Site Details				
Site Area:	0.461 ha			
% Impervious:				
Rational C:	0.60			
Rainfall Station:	Ottawa, ONT			
Particle Size Distribution:	Fine			
Peak Flowrate:				



Notes:

Removal efficiencies are based on NJDEP Test Protocols and independently verified.

All units supplied by ADS have numerous local, provincial, and international certifications (copies of which can be provided upon request). The design engineer is responsible for ensuring compliance with applicable regulations.



Project Name: 53 Craig St

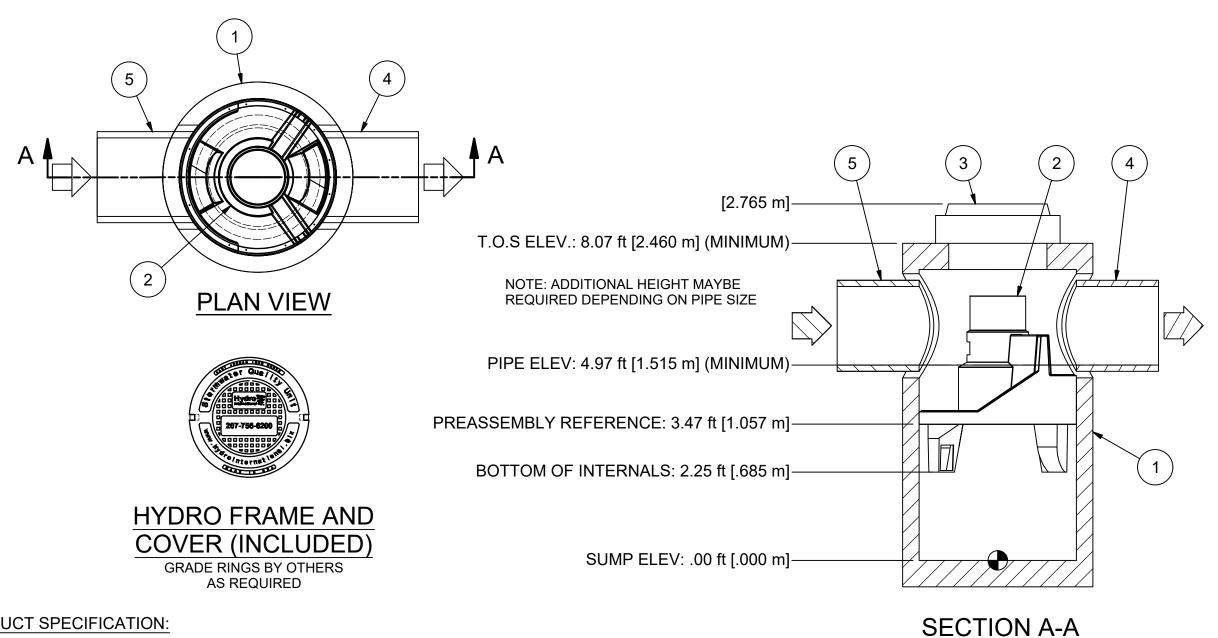
Consulting Engineer: Robinson Consultants Inc

Location: Perth, Ontario

Net Annual Removal Efficiency Summary: FD-4HC

Rainfall Intensity ⁽¹⁾	Fraction of Rainfall ⁽¹⁾	FD-4HC Removal Efficiency ⁽²⁾	Weighted Net-Annual Removal Efficiency	
mm/hr	%	%	%	
0.50	0.1%	100.0%	0.1%	
1.00	14.1%	100.0%	14.1%	
1.50	14.2%	100.0%	14.2%	
2.00	14.1%	99.9%	14.1%	
2.50	4.2%	97.9%	4.1%	
3.00	1.5%	96.2%	1.4%	
3.50	8.5%	94.8%	8.1%	
4.00	5.4%	93.7%	5.1%	
4.50	1.2%	92.7%	1.1%	
5.00	5.5%	91.8%	5.1%	
6.00	4.3%	90.2%	3.9%	
7.00	4.5%	88.9%	4.0%	
8.00	3.1%	87.8%	2.7%	
9.00	2.3%	86.9%	2.0%	
10.00	2.6%	86.0%	2.2%	
20.00	9.2%	80.7%	7.5%	
30.00	2.6%	77.7%	2.0%	
40.00	1.2%	75.6%	0.9%	
50.00	0.5%	74.1%	0.4%	
100.00	0.7%	69.4%	0.5%	
150.00	0.1%	66.9%	0.0%	
200.00	0.0%	65.1%	0.0%	
	Total Net Annu	ual Removal Efficiency:	93%	
	Total Runoff Volume Treated:			

- (1) Rainfall Data: 1960:2007, HLY03, Ottawa, ONT, 6105976 & 6105978.
- (2) Based on third party verified data and appoximating the removal of a PSD similar to the STC Fine distribution
- (3) Rainfall adjusted to 5 min peak intensity based on hourly average.



PRODUCT SPECIFICATION:

- 1. PEAK HYDRAULIC FLOW: 18.0 cfs (510 l/s)
- 2. MIN SEDIMENT STORAGE CAPACITY: 0.7 cu. yd. (0.5 cu. m.)
- 3. OIL STORAGE CAPACITY: 191 gal. (723 liters)
- 4. MAXIMUM INLET/OUTLET PIPE DIAMETERS: 24 in. (600 mm)
- 5. THE TREATMENT SYSTEM SHALL USE AN INDUCED VORTEX TO SEPARATE POLLUTANTS FROM STORMWATER RUNOFF.
- 6. FOR MORE PRODUCT INFORMATION INCLUDING REGULATORY ACCEPTANCES, PLEASE VISIT

https://hydro-int.com/en/products/first-defense

GENERAL NOTES:

- 1. General Arrangement drawings only. Contact Hydro International for site specific drawings.
- 2. The diameter of the inlet and outlet pipes may be no more than 24".
- 3. Multiple inlet pipes possible (refer to project plan).
- 4. Inlet/outlet pipe angle can vary to align with drainage network (refer to project plan.s)
- 5. Peak flow rate and minimum height limited by available cover and pipe diameter.
- 6. Larger sediment storage capacity may be provided with a deeper sump depth.

	PARTSLIST				
ITEM	QTY	SIZE (in)	SIZE (mm)	DESCRIPTION	
1	1	48	1200	I.D. PRECAST MANHOLE	
2	1			INTERNAL COMPONENTS	
				(PRE-INSTALLED)	
3	1	30	750	FRAME AND COVER (ROUND)	
4	1	24 (MAX)	600 (MAX)	OUTLET PIPE (BY OTHERS)	
5	1	24 (MAX)	600 (MAX)	INLET PIPE (BY OTHERS)	

DADTOLICE

PROJECTION



IF IN DOUBT ASK

- MANHOLE WALL AND SLAB THICKNESSES ARE NOT TO SCALE.
- 2. CONTACT HYDRO INTERNATIONAL FOR A BOTTOM OF STRUCTURE ELEVATION PRIOR TO SETTING FIRST DEFENSE MANHOLE.
- 3. CONTRACTOR TO CONFIRM RIM. PIPE INVERTS. PIPE DIA. AND PIPE ORIENTATION PRIOR TO RELEASE OF UNIT TO FABRICATION.

11/8/2019

SCALE: 1:30

DRAWN BY: JLL3

CHECKED BY: APPROVED BY

4-ft DIAMETER

FIRST DEFENSE HIGH CAPACITY

GENERAL ARRANGEMENT



hydro-int.com

HYDRO INTERNATIONAL

DO NOT SCALE DRAWING
STEEL FABRICATION TOLERANCES

 $000 - 012in = \pm 0.04in$ 012 - 024in = +0 06in

 $000 - 120in = +1^{\circ}$ 120 - 240in = ±0.5°

WEIGHT:

048 - 120in = ±0.12in

N/A

STOCK NUMBER:

4FDHC FDHC GA STD

SHEET SIZE: SHEET:

1 OF 1

MATERIAL:

ANY WARRANTY GIVEN BY HYDRO INTERNATIONAL WILL APPLY ONLY TO THOSE ITEMS SUPPLIED BY IT. ACCORDINGLY HYDRO INTERNATIONAL CANNOT ACCEPT ANY RESPONSIBILITY FOR ANY STRUCTURE, PLANT, OR EQUIPMENT, (OR THE PERFORMANCE THERE OF) DESIGNED, BUILT, MANUFACTURED, OR SUPPLIED BY ANY THIRD PARTY, HYDRO INTERNATIONAL HAVE A POLICY OF CONTINUOUS DEVELOPMENT AND RESERVE THE RIGHT TO AMEND THE SPECIFICATION, HYDRO INTERNATIONAL CANNOT ACCEPT LIABILITY FOR PERFORMANCE OF ITS EQUIPMENT, (OR ANY PART THEREOF), IF THE EQUIPMENT IS SUBJECT TO CONDITIONS OUTSIDE ANY DESIGN